An Update on Stormwater Management Regulation in Virginia

Wetland Studies and Solutions, Inc.

5300 Wellington Branch Drive · Suite 100 Gainesville, Virginia 20155 www.wetlandstudies.com

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VA Stormwater Management Regulations

Timeline

2010

• **Spring 2010**: HB 1220 and SB 395 delay regulations until 280 days after approval of the TMDL but no later than December 1, 2011.

2011

- May 24: Board adopted final regulations
- June 20 August 2: Administration review
- August 10: Deadline for submittal of regulatory materials to registrar for publication
- August 29: Publication in Virginia Registrar, start of final adoption period
- **September 12**: Final adoption period closes
- **September 13:** Statutory effective date target

2014

• July 1: Implementation date



VA Stormwater Management Regulations

Major Elements

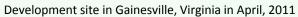
- Grandfathering (4VAC50-60-48)
- Stormwater Pollution Prevention Plan Requirements (Effluent Limit Guidelines; 4VAC50-60-54.F)
- Quality (4VAC50-60-63)
- Quantity (4VAC50-60-66)
- Offsite Compliance Options (4VAC50-60-69)

Note: Information contained in this presentation represents the version of the Stormwater Regulations that became effective on September 13, 2011 (available at http://www.dcr.virginia.gov/documents/swmfinregspublishedvareg.pdf).



Grandfathering





Grandfathering

Overview

- After July 1, 2009, sites with VSMP permit shall be covered under existing permit criteria for additional 2 permits (after June 30, 2014 expiration; 4VAC50-60-47.1)
- Until June 30, 2019, land disturbing activity (with conditions below) approved by locality by July 1, 2012 and no VSMP permit by July 1, 2014 (4VAC50-60-48.A)
 - Conditions: Proffered or conditional zoning plan, preliminary or final subdivision plat, preliminary or final site plan, or zoning with a plan of development
 - Grandfathered until June 30, 2019 (4VAC50-60-48.C)
- Project with issued governmental bonding or public debt financing by July 1, 2012 (4VAC50-60-48.B)
 - Grandfathered until June 30, 2019 (4VAC50-60-48.C)



SW Pollution Prevention Plan Reqs.



Stream in Arlington, Virginia, on 6/27/10

(Source: Aileen Winquist - Arlington County)

SW Pollution Prevention Plan Reqs.

Verbatim from the Regulations

NTU requirements (were 280 NTUs) removed due to lawsuit, but EPA still required DCR to add the following (verbatim):

4VAC50-60-54. Stormwater pollution prevention plan requirements.

- F. The stormwater pollution prevention plan must address the following requirements, to the extent otherwise required by state law or regulations and any applicable requirements of a VSMP permit:
 - **1. Control stormwater volume and velocity** within the site to minimize soil erosion;
 - **2. Control stormwater discharges**, including both peak flow rates and total stormwater volume, to minimize erosion at outlets and to minimize downstream channel and stream bank erosion;







SW Pollution Prevention Plan Reqs.— cont.

Verbatim from the Regulations

4VAC50-60-54. Stormwater pollution prevention plan requirements.

- 3. Minimize the amount of soil exposed during construction activity;
- 4. Minimize the disturbance of steep slopes;
- 5. Minimize sediment discharges from the site.

 design, installation and maintenance of erosion and sediment controls must address factors such as the amount, frequency, intensity and duration of precipitation, the nature of resulting stormwater runoff, and soil characteristics, including the range of soil particle sizes expected to be present on the site;



E&S Inspection

6. Provide and maintain natural buffers around surface waters, direct stormwater to vegetated areas to increase sediment removal and maximize stormwater infiltration, unless infeasible;

SW Pollution Prevention Plan Reqs.

What does this mean?

4VAC50-60-54. Stormwater pollution prevention plan requirements.

- 7. Minimize soil compaction and, unless infeasible, preserve topsoil; and
- 8. Stabilization of disturbed areas must, at a minimum, be initiated immediately whenever any clearing, grading, excavating, or other earth disturbing activities have permanently ceased on any portion of the site, or temporarily ceased on any portion of the site and will not resume for a period exceeding 14 calendar days.



E&S Inspection

This may be a problem because E & S plans and regulations don't appear to meet all of the requirements (although this is debatable).

Water Quality

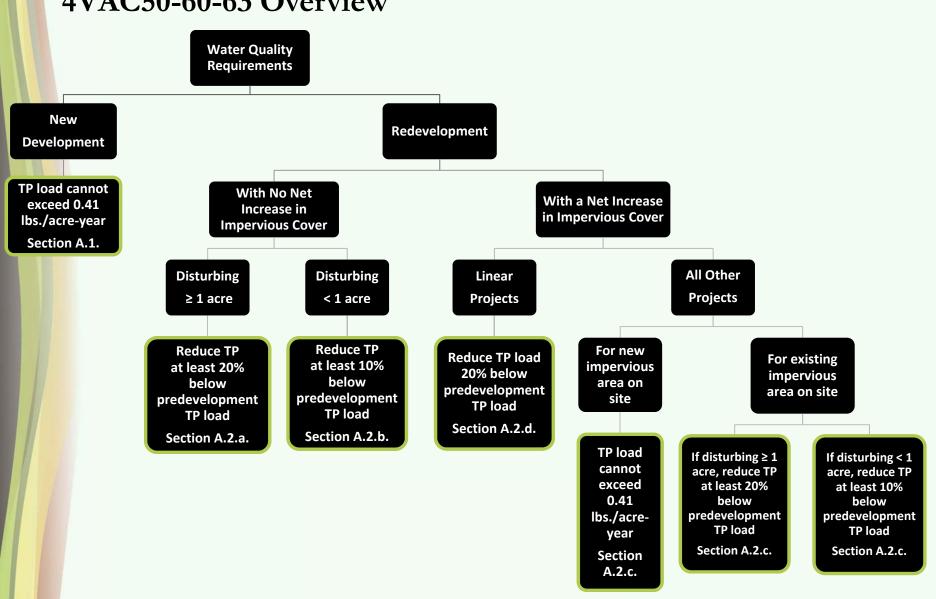


Algae blooms near Norfolk Yacht Club on 8/8/09

(Source: Ryan C. Henriksen – The Virginian Pilot)

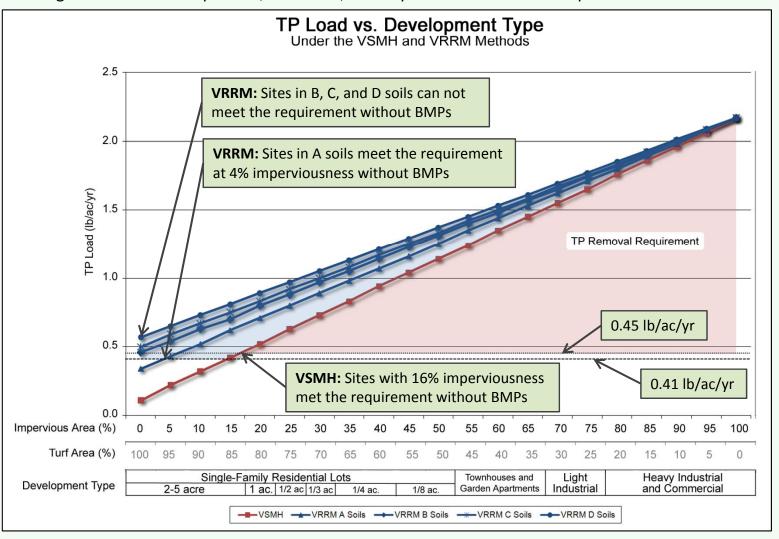
Water Quality

4VAC50-60-63 Overview



Comparing the new 0.41 lb/ac/yr to the old 0.45 lb/ac/yr

The loading rates are not comparable; therefore, the requirements are not comparable either!



Comparing the new 0.41 lb/ac/yr to the old 0.45 lb/ac/yr

Why the difference in loading-rate calculations?

VSMH: Under the VSMH, TP loads were calculated using the Simple Method.

The old regulations required a loading rate of 0.45 lb/ac/yr based on a calculation of average land cover (excluding urban) and loading rates, as follows:

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F_{va} = relative total phosphorus load for Virginia's Chesapeake Bay Watershed = (%forest x F_{forest}) + (%pasture x F_{pasture}) + (%conservation till x F_{cons. till}) + (%conventional till x F_{conv. till}) = (0.66 x 0.12) + (0.21 x 0.59) + (0.07 x 1.52) + (0.06 x 2.42) = 0.45 lb/ac/yr
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(See the Chesapeake Bay Local Assistance Department's Local Assistance Manual, November 1989.)

VRRM: The VRRM calculates loading rates based on a modified Simple Method which accounts for soil types as well as for TP loads from forested land and turf.

The new regulations require a loading rate of 0.41 lb/ac/yr based on the discussion on the following slides. (See slides 14-17.)

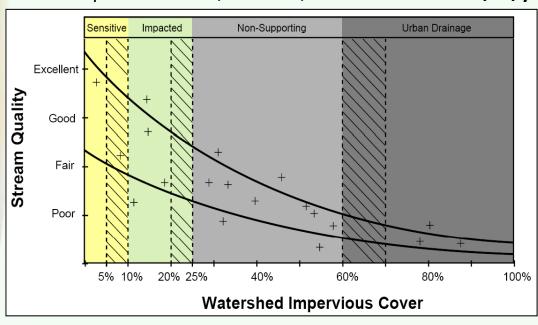
Why $0.41 \, lb/ac/yr$?

How should the allowable loading rate be calculated state-wide?

- The subcommittee recommended 0.36 lb/ac/yr TP based on a Modified VRRM calculation (to account for forest):
 - Assumes 7.5% impervious cover¹, 30% turf, and 62.5% VA-average forest cover
 - Assumes 1.15% HSG A, 61.28% HSG B, 28.60% HSG C, and 8.97% HSG D²

Other Options:

- 10% impervious cover, 30% turf, 60% forest = 0.41 lb/ac/yr
- 5% impervious cover, 30% turf, 65% forest = 0.30 lb/ac/yr



- [1] Schueler, T., Fraley-McNeal, L., and Cappiella, K. "Is Impervious Cover Still Important? Review of Recent Research." Journal of Hydrologic Engineering, April, 2009.
- ^[2] Weighted average soil cover was derived from STATSGO state-wide soils database soils breakdown for Virginia outside of the Chesapeake Bay Watershed. STATSGO breakdown: 210 mi² HSG A; 0 mi² HSG A/D; 11,207 mi² HSG B; 0 mi² HSG B/D; 5,231 mi² HSG C; 373 mi² HSG C/D; 1,153 mi² HSG D; 115 mi² Unrated. C/D and unrated soils were assigned to HSG D.

Why 0.41 lb/ac/yr? (cont.)

Jantz, P., Goetz, S., and Jantz, C. 2005. *Urbanization and the Loss of Resource Lands in the Chesapeake Bay Watershed*. Journal of Environmental Management. 36 (6): 808-825.

Page 823 -

In our most conservative estimate, we calculate that at least 388 km² of forest lands, 1,016 km² of agricultural lands, and 2 km² of wetlands, have been lost to commercial and residential development within the CBW since 1990. As much as 826 km² of forests, 1,543 km² of agricultural lands, and 60 km² of wetlands have been converted, although we emphasize the more moderate results derived from the land cover agreement map indicating losses of 504 km² for forests, 1,266 km² for agricultural lands, and 2 km² for wetlands. However, we would expect functional losses,

Chesapeake Bay Watershed:

Conservative Estimate $388 + 1,016 + 2 = 1,406 \text{ km}^2 \text{ converted}$ 390 / 1,406 = 28% converted from forest (with wetlands) 1,106 / 1,406 = 72% converted from agriculture

Unconservative Estimate

826 + 60 + 1,543 = 2,429 km² converted 886 / 2,429 = **36**% converted from forest (with wetlands) 1,543 / 2,429 = **64**% converted from agriculture

Moderate Estimate

 $504 + 1,266 + 2 = 1,772 \text{ km}^2 \text{ converted}$ 506 / 1,722 = 29% converted from forest (with wetlands)1,266 / 1,722 = 71% converted from agriculture



Why $0.41 \, lb/ac/yr$? (cont.)

Based on historic development trends per Jantz et. al, **TP = 0.51 to 0.56 lb/ac/yr** to achieve no-net-increase above the allowable average 2025 nutrient loads from previous land uses per the November 2010 WIP.

TP Load Based on Varying Percentages of Previous Land Uses Converted to Development										
		Forest TP Load		Agriculture TP	Total TP Load					
Source ¹	% Forest	(lb/ac/yr) ²	% Agriculture	Load (lb/ac/yr) ²	(lb/ac/yr) ³					
Conservative Estimate	28%		72%		0.56					
Unconservative Estimate	36%	0.11	64%	0.74	0.51					
Moderate Estimate	29%		71%		0.56					

- 1. Historic development trends were derived from: Jantz, P., Goetz, S., and Jantz, C. 2005. *Urbanization and the Loss of Resource Lands in the Chesapeake Bay Watershed*. Journal of Environmental Management. 36 (6): 823.
- 2. Calculated as the draft WIP 2025 forest and agricultural allocations divided by 2010 sector acreages (which were transmitted to WSSI via e-mail from Russ Perkinson on 8/12/2010).

(For forest: 1,072,000 lb/yr / 9,776,274 ac = 0.11 lb/ac/yr. For agriculture: 2,097,000 lb/yr / 2,836,970 ac = 0.74 lb/ac/yr)

3. Total TP Load is calculated as the sum of (% Forest x Forested TP Load + % Agriculture x Agriculture TP Load)





Why 0.41 lb/ac/yr? (cont.)

November 2010 Final Phase I Virginia WIP:

"The Tier 1 load-balancing approach uses the allocation loads for forest, cropland, pasture, and hay land uses in the Chesapeake Bay Program's Phase 5.3 Watershed Model to calculate the average pollutant loads from a generic pre-development acre based on the mix of projected land to be developed for Virginia's Chesapeake Bay watershed." (Final WIP, pg. 86)

State-wide Requirement Based on Percentage of Impervious Cover and STATSGO average soil cover		Current Compromise	Chesapeake Bay Requirement Based on "No Increase" from previous land uses		
5% impervious, 65% forest, 30% turf	0.30		0.51	36% forest, 64% agriculture	
7.5% impervious, 62.5% forest, 30% turf	0.36 0.41		0.56	28% forest, 72% agriculture	
10% impervious, 60% forest, 30% turf	0.41		0.56	29% forest, 71% agriculture	



Why 10% and 20% Reductions for Redevelopment?

The Chesapeake Bay Preservation Act previously required a TP load reduction of 10% for redeveloped sites.

The new regulations sought to improve over current conditions without discouraging redevelopment; therefore, the SAG agreed on a 20% TP load reduction requirement for redeveloped sites.

However, a 20% TP load reduction is difficult for small sites, so the previous 10% TP load reduction requirement was maintained for sites <1 ac.



Water Quality - cont.

What does this mean for new development?

This means more BMPs and more infiltration (where possible).

For example in Fairfax County, consider:

A downtown commercial site on C soils (80% impervious and 20% turf)

Under the old regulations, the site produces: 1.76 lb/ac/yr TP

Under the old regulations, the load must be reduced by 40% to: 1.06 lb/ac/yr TP

This currently can be done with extended detention ponds.



Extended detention pond



Extended detention pond

Water Quality - cont.

What does this mean for new development?

Same site:

A downtown commercial site on C soils (80% impervious and 20% turf)

Under the new regulations, the site produces:

1.83 lb/ac/yr TP
Under the new regulations, the load must be reduced by 78% to:

0.41 lb/ac/yr TP

• This cannot be accomplished with extended detention alone; requires additional BMPs (rain gardens, cisterns, permeable pavements, infiltration, wetlands, etc.) or trading.

The debate on trading is ongoing:

- Who sets the price of credits- the market or the government?
- How much can be traded? What percentage must be achieved on-site?
- How will acceptable service areas be determined?



Pervious pavers



Cistern

Quantity Control



Snakeden Branch in Reston, Virginia, prior to restoration

Quantity Control

4VAC50-60-66 Overview

4VAC50-60-66 requires the energy balance method on the 1-year storm event.

• Executive Order 13508 requires developers to match pre-development hydrology. The energy balance method provides a practical solution for sites that can not meet pre-development hydrology.

4VAC50-60-66 defines requirements for three outfall conditions:

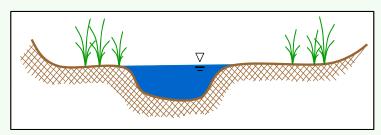
- Manmande conveyance systems;
- Restored conveyance systems; and
- Natural conveyance systems.



Energy Balance

The theory behind 4VAC50-60-66.B

- Stable streams in this region and climatic epoch formed in forested watersheds and achieve stability by overbank flooding in the 1-1.5 year event.
- To prevent degradation, need to match peak flow, volume, and timing of such conditions.

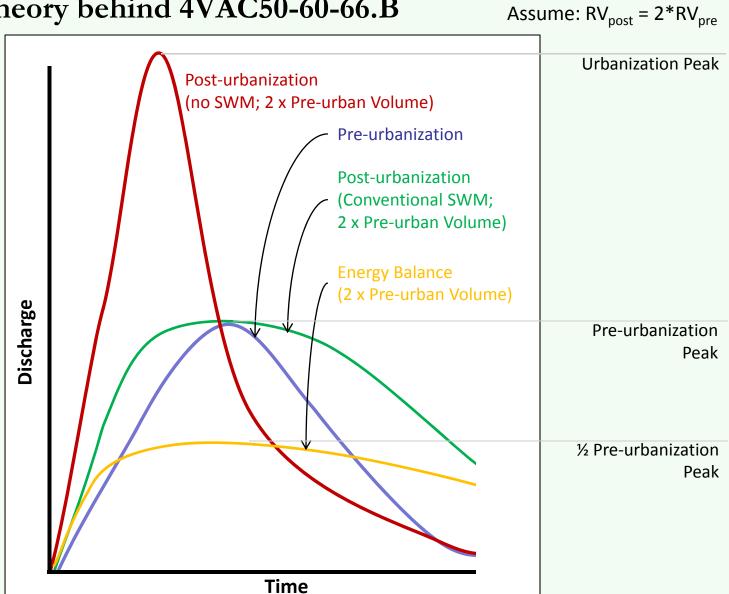


Stream cross section at bankfull stage

- Traditional SW management controls peak flow, but increases volume, which increases stream power (and power degrades streams).
- Goal of the energy balance method:
 - Keeps pre-development power same by reducing peak flow rate if volume increases;
 - Provides a quantifiable incentive to match pre-development volume to the MEP; and
 - Mass Balance Equation: Q*Rv_{post} = Q*RV_{forest}
- Economic considerations of proposed version use pre-development conditions instead of forest (unlike state law and Fairfax County PFM), coupled with improvement factor, I.F. (The I.F. is required because state law requires an improvement on existing conditions.)
 - I.F. of 0.8 yields same ballpark SW sizing as forest conditions

Energy Balance

The theory behind 4VAC50-60-66.B



24

Energy Balance

The theory behind 4VAC50-60-66.B

Energy Balance Method:



Restored conveyance system

Allowable 1-yr, 24-hr peak flow rate:

 $Q_{developed} \leq I.F. \times Q_{pre-developed} \times RV_{pre-developed} / RV_{developed}$

 $Q_{developed}$ shall not be required to be less than $[Q_{forested} \times RV_{forested}] / Rv_{developed}$

 $Q_{developed}$ must be $\leq Q_{pre-developed}$

- Q = Peak flow rate of runoff
- RV = Volume of runoff
- Improvement Factor (I.F.) = 0.8 for sites > 1 ac 0.9 for sites < 1 ac
- Pre-developed = conditions prior to development, not pre-colonial conditions



Natural conveyance system



Quantity Control

4VAC50-60-66.B.1

Outfall condition 1: Manmade conveyance systems

- 1. Convey the 2-year, 24-hour storm (after SWM) without erosion, OR
- 2. Allowable 1-yr, 24-hr peak flow rate for all conditions:
 - $Q_{developed} \leq IF \times Q_{pre-developed} \times RV_{pre-developed} / RV_{developed}$
 - Q_{developed} shall not be required to be less than [Q_{forested} x RV_{forested}] / Rv_{developed}
 - $Q_{developed}$ must be $\leq Q_{pre-developed}$

- Q = Peak flow rate of runoff
- RV = Volume of runoff
- Improvement Factor (IF) = 0.8 for sites > 1 ac
 0.9 for sites < 1 ac
- Pre-developed = conditions prior to development, not pre-colonial conditions



Manmade conveyance system

Quantity Control - cont.

4VAC50-60-66.B.2

Outfall condition 2: Restored conveyance systems

- 1. Discharge was considered in the design of the restored system, OR
- 2. Allowable 1-yr, 24-hr peak flow rate for all conditions:
 - $Q_{developed} \leq IF \times Q_{pre-developed} \times RV_{pre-developed} / RV_{developed}$
 - Q_{developed} shall not be required to be less than [Q_{forested} x RV_{forested}] / Rv_{developed}
 - Q_{developed} must be ≤ Q_{pre-developed}

- Q = Peak flow rate of runoff
- RV = Volume of runoff
- Improvement Factor (IF) = 0.8 for sites > 1 ac 0.9 for sites ≤ 1 ac
- Pre-developed = conditions prior to development, not pre-colonial conditions



Restored conveyance system



Quantity Control - cont.

4VAC50-60-66.B.3

Outfall condition 3: Natural conveyance systems

Allowable 1-yr, 24-hr peak flow rate for all conditions:

- $Q_{developed} \leq IF \times Q_{pre-developed} \times RV_{pre-developed} / RV_{developed}$
- Q_{developed} shall not be required to be less than [Q_{forested} x RV_{forested}] / Rv_{developed}
- Q_{developed} must be ≤ Q_{pre-developed}

- Q = Peak flow rate of runoff
- RV = Volume of runoff
- Improvement Factor (IF) = 0.8 for sites > 1 ac
 0.9 for sites < 1 ac
- Pre-developed = conditions prior to development, not pre-colonial conditions



Natural conveyance system

Quantity Control - cont.

Limits of Analysis (4VAC50-60-66.B.4)

Stormwater conveyance systems shall be analyzed for channel protection to a point where either one of the following is satisfied:

1. <u>Based on area</u>

Prior to any land disturbance, the site's contributing drainage area to site discharge point is $\leq 1.0\%$ of total watershed area draining to that point of discharge, or

2. Based on peak flow rate

Based on peak flow rate, the site's peak flow rate from the one-year 24-hour storm is less than or equal to 1.0% of the existing peak flow rate from the one-year 24-hour storm prior to the implementation of any stormwater quantity control measures.



Flood Protection

4VAC50-60-66.C

For stormwater conveyance systems* that currently do not experience localized flooding during the 10-year, 24-hour storm event:

• Confine the post-development peak flow rate from the 10-year, 24-hour storm event within the stormwater conveyance system.

For stormwater conveyance systems* that currently do experience localized flooding during the 10-year, 24-hour storm event:

- Confine the post-development peak flow rate from the 10-year, 24-hour storm event within the stormwater conveyance system; or
- Release a post-development peak flow rate for the 10-year, 24-hour storm event that is less than the pre-development peak flow rate from the 10-year, 24-hour storm event.

^{*} See next slide

Flood Protection

4VAC50-60-66.C

- * 4VAC50-60-10. Definitions:
- "Stormwater conveyance system" means a combination of drainage components that are used to convey stormwater discharge, either within or downstream of the land-disturbing activity. This includes:
- 1. "Manmade stormwater conveyance system" means a pipe, ditch, vegetated swale, or other stormwater conveyance system constructed by man except for restored stormwater conveyance systems;
- 2. "Natural stormwater conveyance system" means the main channel of a natural stream and the flood-prone area adjacent to the main channel; or
- 3. "Restored stormwater conveyance system" means a stormwater conveyance system that has been designed and constructed using natural channel design concepts. Restored stormwater conveyance systems include the main channel and the flood-prone area adjacent to the main channel.
- "Flood-prone area" means the component of a natural or restored stormwater conveyance system that is outside the main channel. Flood-prone areas may include, but are not limited to, the floodplain, the floodway, the flood fringe, wetlands, riparian buffers or other areas adjacent to the main channel.
- "Floodplain" means the area adjacent to a channel, river, stream, or other water body that is susceptible to being inundated by water associated with the 100-year flood or storm event. This includes, but is not limited to, the floodplain designated by the Federal Emergency Management Agency.
- "Floodway" means the channel of a river or other watercourse and the adjacent land areas, usually associated with flowing water, that must be reserved in order to discharge the 100-year flood or storm event without cumulatively increasing the water surface elevation more than one foot. This includes, but is not limited to, the floodway designated by the Federal Emergency Management Agency.
- "Flood fringe" means the portion of the floodplain outside the floodway that is usually covered with water from the 100-year flood or storm event. This includes, but is not limited to, the flood or floodway fringe designated by the Federal Emergency Management Agency.

Quantity Control

Summary

- Requires the Energy Balance of the 1-year, 24-hour storm with I.F. and no increase in 10- year peak flows, rather than conventional 2- and 10-year peak flow analysis;
- No longer requires Adequate Outfall (MS-19)
 - 4VAC50-60-66.A: "Compliance with the minimum standards set out in this section shall be deemed to satisfy the requirements of 4VAC50-30-40.19"
- Pond footprints will typically be similar (±15%) because the 10-year Flood Protection governs
 the overall size (which matches most current requirements);
- The size of the 2-year orifice will be reduced to meet 1-year Energy Balance requirement; and
- The 1-year detention volume will usually be greater than the current 2-year volume requirement.

Will result in the more effective use of SWM facilities to protect streams and reduce erosion/sediment at minimal cost.



Offsite Compliance Options





Offsite Compliance

Overview

- Off-site compliance options include:
 - Adopted comprehensive watershed SW management plan in local watershed of project
 - Locality pollutant loading pro rata share program
 - Nonpoint nutrient offset program established by VA Code
 - Other options approved by applicable state agency or board
 - Other properties within same or upstream HUC can be used to meet project TP reductions
- Offsite compliance options must meet only one of the following:
 - At least 75% of required phosphorus nutrient reductions are achieved on-site;
 - < 5 acres of land will be disturbed; or
 - Post construction phosphorus control requirement is < 10 pounds per year.
- Local SW management programs may develop comprehensive SW management plans to be approved by the department
- Senate Bill 1099 (2011 Session) addresses SW nonpoint nutrient offsets and establishes priorities to be used by permit issuing authorities
- HB176/SB77 (2012 Session) modify requirements.



Virginia Stormwater BMP Clearinghouse

4VAC50-60-65.B

Administered by DCR and the Virginia Water Resources Research Center at Virginia Tech, and overseen by a stakeholders' committee

Purpose:

- To disseminate design standards and specifications for all stormwater BMPs approved for use in Virginia;
- To disseminate the evaluation and performance certification of proprietary BMPs approved for use in Virginia; and
- To provide information and links to related websites.

4VAC50-60-65.B: "The BMPs listed in this subsection are approved for use as necessary to effectively reduce the phosphorus load and runoff volume in accordance with the Virginia Runoff Reduction Method. Other approved BMPs found on the Virginia Stormwater BMP Clearinghouse Website at http://www.vwrrc.vt.edu/swc may also be utilized. Design specifications and the pollutant removal efficiencies for all approved BMPs are found on the Virginia Stormwater BMP Clearinghouse Website at http://www.vwrrc.vt.edu/swc."



http://wrrc.vt.edu/swc/StandardsSpecs.html

Website Screenshot



Runoff Reduction and Nutrient Removal Comparison

Two design levels:

Level 1

- Typically less strict design requirements;
- Typically lower runoff reduction; and
- Typically lower EMC removal.

Level 2

- Typically stricter design requirements;
- Typically higher runoff reduction; and
- Typically higher EMC removal.

Practice	Table 1	Table 1. Comparative Runoff Reduction and Nutrient Removal for Practices						
Disconnect Sheet Flow to Veg. Filter or Conserv. Open Space 25 50 to 75 0 50 to 75		Design Level	Runoff Reduction	TN EMC	TN Mass Load Removal	TP EMC	TP Mass Load Removal ⁶	
Sheet Flow to Veg. Filter or Conserv. Open Space 1		12	25 to 50 ¹	7.52		0	25 to 50 ¹	
to Veg. Filter or Conserv. Open Space Grass				No Leve	el 2 Design			
Open Space	to Veg. Filter	1	50	o	50	0	50	
Channels	Open Space			100		1911	1000 000 000	
Can be used to Decrease Runoff Coefficient for Turf Cover at Site. See the design's ecs for Rooftop Disconnection, Sheet Flow to Vegetated Filter or Conserved dopen Space, and Grass Channel Vegetated Roof		1	10 to 20 1			15	24 to 41 '	
Compost Amendment	Channels	-						
Roof 2 60 0 60 0 60 0 60 Rainwater Harvesting 1 Up to 90 3,5 0 Up to 90 3,5 0	Compost Amendment	design s	ecs for Rooftop	Disconnection	n, Sheet Flow			
Rainwater Harvesting				-				
Harvesting	Roof			-				
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Bioretention No Level 2 Design	Practices	2	80	60	90	50	90	
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Swales 2 0 35 35 40 40 Filtering Practices 1 0 30 30 60 60 Constructed Vetlands 1 0 25 25 50 50 Wet Vetlands 2 0 55 55 75 75 Wet Ponds 1 0 30 (20) 4 30 (20) 4 50 (45) 4 50 (45) 4 Ponds 2 0 40 (30) 4 40 (30) 4 75 (65) 4 75 (65) 4 Ext. Det. 1 0 10 10 15 15	Swales	2	60	35	74	40	76	
Filtering 1 0 30 30 60 60 For actices 2 0 45 45 65 65 Constructed 1 0 25 25 50 50 Wetlands 2 0 55 55 75 75 75 Wet 1 0 30 (20) 4 30 (20) 4 50 (45) 4 50 (45) 4 Ponds 2 0 40 (30) 4 40 (30) 4 75 (65) 4 75 (65) 4 Ext. Det. 1 0 10 10 15 15	Wet	1	0	25	25	20	20	
Practices 2 0 45 45 65 65 Constructed Wetlands 1 0 25 25 50 50 Wet 1 0 30 (20) 4 30 (20) 4 50 (45) 4 50 (45) 4 Ponds 2 0 40 (30) 4 40 (30) 4 75 (65) 4 75 (65) 4 Ext. Det. 1 0 10 10 15 15	Swales	2	0	35	35	40	40	
Practices 2 0 45 45 65 65 Constructed Wetlands 1 0 25 25 50 50 Wet 1 0 30 (20) 4 30 (20) 4 50 (45) 4 50 (45) 4 Ponds 2 0 40 (30) 4 40 (30) 4 75 (65) 4 75 (65) 4 Ext. Det. 1 0 10 10 15 15	Filtering	1	0	30	30	60	60	
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Wet 1 0 30 (20) 4 30 (20) 4 50 (45) 4 50 (45) 4 Ponds 2 0 40 (30) 4 40 (30) 4 75 (65) 4 75 (65) 4 Ext. Det. 1 0 10 10 15 15	Constructed	1	0	25	25	50	50	
Ponds 2 0 40 (30) 4 40 (30) 4 75 (65) 4 75 (65) 4 Ext. Det. 1 0 10 10 15 15	Wetlands	2	0	55	55	75	75	
Ponds 2 0 40 (30) 4 40 (30) 4 75 (65) 4 75 (65) 4 Ext. Det. 1 0 10 10 15 15	Wet	1	0	30 (20) 4	30 (20) 4	50 (45) ⁴	50 (45) ⁴	
Ext. Det. 1 0 10 10 15 15	Ponds	2	0	40 (30) 4	40 (30) 4	75 (65) ⁴		
	Ext. Det.	1	0		10			
101103 2 10 10 24 15 37	Ponds	2	15	10	24	15	31	

Specification No. 1: Impervious Surface Disconnection

What is it?

Eliminating direct connections between impervious surfaces and the storm sewer. May be a simple disconnection or a disconnection to an alternative practice.

Simple disconnection directs runoff to pervious areas, providing volume reduction but no

additional nutrient removal.

Disconnection to alternative BMP may enhance removal rates. Alternative BMPs include:

- Compost-amended soil;
- Dry well or French drain;
- Rain garden;
- Cistern; or
- Stormwater planters



Impervious surface disconnection Source: DCR Stormwater Design Spec No. 1

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Impervious Surface	1	25 to 50	0	25 to 50	0	25 to 50
Disconnection	No Level 2 Design					

Specification No. 1: Impervious Surface Disconnection (cont.)

Stormwater Functions Summary

Table 1.1. Summary of Stormwater Functions Provided by Rooftop Disconnection 1

FUNCTION DECLEDED BY CHARLE	1100 0011 0 0 1 1 1			
FUNCTION PROVIDED BY SIMPLE	HSG SOILS A and B	HSG SOILS C and D		
ROOFTOP DISCONNECTION		III		
Annual Runoff Volume Reduction (RR)	50%	25%		
Total Phosphorus (TP) EMC Reduction by	0	0		
BMP Treatment Process	U	· ·		
Total Phosphorus (TP) Mass Load Removal	50%	25%		
Total Nitrogen (TN) EMC Reduction by BMP	0	0		
Treatment Process	0	U		
Total Nitrogen (TN) Mass Load Removal	50%	25%		
	Partial: Designers can us	e the RRM spreadsheet		
Channel & Flood Protection	to adjust curve number for each design storm for			
Gilaillei & Flood Flotection	the contributing drainage area (CDA), based on			
	annual runoff reduction ach	nieved		

NOTE: Stormwater functions of disconnection can be boosted if an acceptable alternative runoff reduction practice is employed. Acceptable practices and their associated runoff reduction rates are listed below. Designers should consult the applicable specification number for design standards.

Alternative Practice	Specification No.	Runoff Reduction Rate
Soil compost-amended filter path	4	50%
Dry well or french drain #1 (Micro-infiltration #1)	8	50%
Dry well or french drain #2 (Micro-infiltration #2)	8	90%
Rain garden #1, front yard bioretention (Micro-	9	40%
bioretention #1)		
Rain garden #2, front yard bioretention (Micro-	9	80%
bioretention #2)		
Rainwater harvesting	6	Defined by user
Stormwater Planter (Urban Bioretention)	9 (Appendix A)	40%
¹ CWP and CSN (2008), CWP (2007)	_	

Design Criteria

Table 1.2: Simple Rooftop	Disconnection D	esign Criteria 1
---------------------------	-----------------	------------------

DESIGN FACTOR	SIMPLE DISCONNECTION
Maximum impervious (Rooftop) Area Treated	1,000 sq. ft. per disconnection
Longest flow path (roof/gutter)	75 feet
Disconnection Length	Equal to longest flow path, but no less than 40 feet ²
Disconnection slope	< 2%, or < 5% with turf reinforcement 3
Distance from buildings or foundations	Extend downspouts 5 ft. 4 (15 ft. in karst areas) away from building <i>if grade is less than 1%</i> .
Type of Pretreatment	External (leaf screens, etc)

¹ For alternative runoff reduction practices, see the applicable specification for design criteria. See Table 1 in this specification for eligible practices and associated specification numbers.

² An alternative runoff reduction practice must be used when the disconnection length is less than 40 feet.

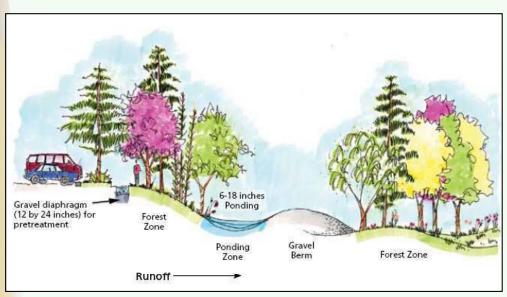
³ Turf reinforcement may include EC-2, EC-3, or other appropriate reinforcing materials that are confirmed by the designer to be non-erosive for the specific characteristics and flow rates anticipated at each individual application, and acceptable to the plan approving authority.

⁴ Note that the downspout extension of 5 feet is intended for simple foundations. The use of a dry well or french drain adjacent to an in-ground basement or finished floor area should be carefully designed and coordinated with the design of the structure's water-proofing system (foundation drains, etc.), or avoided altogether.

Specification No. 2: Sheet Flow

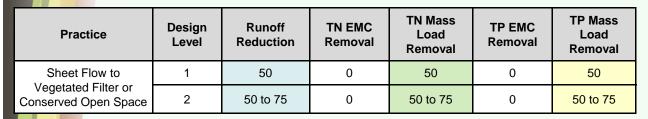
What is it?

Direct sheet flow to conserved open space (to protect vegetated areas adjacent to streams) or to vegetated filter strips (to treat small impervious areas or as pretreatment for another practice).



Typical sheet flow to open space

DCR Stormwater Design Spec No. 2







Sheet flow to open space
Source: DCR Stormwater Design Spec No. 2

Specification No. 2: Sheet Flow (cont.)

Stormwater Functions Summary

Table 2.1: Summary of Stormwater Functions Provided by Filter Strips 1

	Conserva	tion Area	Vegetated Filter Strip		
Stormwater Function	HSG Soils A and B	HSG Soils C and D	HSG Soils A	HSG Soils B ⁴ , C and D	
		no CA ² in Ition Area	No CA 3	With CA ²	
Annual Runoff Vol. Reduction (RR)	75%	50%	50%	50%	
Total Phosphorus (TP) EMC					
Reduction ⁵ by BMP Treatment	()	0		
Process					
Total Phosphorus (TP) Mass Load Removal	75%	50%	50%	50%	
Total Nitrogen (TN) EMC Reduction by BMP Treatment Process	0			0	
Total Nitrogen (TN) Mass Load Removal	75%	50%	50%	50%	
Channel Protection and Flood Mitigation	Partial. Designers can use the RRM spreads adjust curve number for each design storm contributing drainage area; and designers can account for a lengthened T Concentration flow path in computing peak disch				

¹CWP and CSN (2008); CWP (2007)

Design Criteria

Table 2.2. Filter Strip Design Criteria						
Design Issue	Conserved Open Space	Vegetated Filter Strip				
Soil and Vegetative Cover (Sections 6.1 and 6.2)	Undisturbed soils and native vegetation	Amended soils and dense turf cover or landscaped with herbaceous cover, shrubs, and trees				
Overall Slope and Width (perpendicular to the flow) (Section 5)	0.5% to 3% Slope – Minimum 35 ft width 3% to 6% Slope – Minimum 50 ft width The first 10 ft. of filter must be 2% or less in all cases ²	1% ¹ to 4% Slope – Minimum 35 ft. width 4% to 6% Slope – Minimum 50 ft. width 6% to 8% Slope – Minimum 65 ft. width The first 10 ft. of filter must be 2% or less in all cases				
Sheet Flow (Section 5)	Maximum flow length of 150 ft. from ad Maximum flow length of 75 ft. from adj					
Concentrated Flow (Section 6.3)	Length of ELS ⁶ Lip = 13 lin. ft. per each 1 cfs of inflow if area has 90% Cover ³ Length = 40 lin. ft. per 1 cfs for forested or re-forested Areas ⁴ (ELS ⁶ length = 13 lin.ft. min; 130 lin.ft. max.)	Length of ELS ⁶ Lip = 13 lin.ft. per each 1 cfs of inflow (13 lin.ft. min; 130 lni.ft. max.)				
Construction Stage (Section 8)	Located outside the limits of disturbance and protected by ESC controls	Prevent soil compaction by heavy equipment				
Typical Applications (Section 5)	Adjacent to stream or wetland buffer or forest conservation area	Treat small areas of IC (e.g., 5,000 sf) and/or turf-intensive land uses (sports fields, golf courses) close to source				
Compost Amendments (Section 6.1)	No	Yes (B, C, and D soils) 5				
Boundary Spreader (Section 6.3)	GD ⁶ at top of filter	GD ⁶ at top of filter PB ⁶ at toe of filter				

¹ A minimum of 1% is recommended to ensure positive drainage.

² CA = Compost Amended Soils (see Design Specification No. 4)

³ Compost amendments are generally not applicable for undisturbed A soils, although it may be advisable to incorporate them on mass-graded A or B soils and/or filter strips on B soils, in order to maintain runoff reduction rates.

⁴ The plan approving authority may waive the requirement for compost amended soils for filter strips on B soils under certain conditions (see Section 6.2 below)

There is insufficient monitoring data to assign a nutrient removal rate for filter strips at this time.

 $^{^2}$ For Conservation Areas with a varying slope, a pro-rated length may be computed only if the first 10 ft. is 2% or less.

³ Vegetative Cover is described in Section 6.2.

⁴ Where the Conserved Open Space is a mixture of native grasses, herbaceous cover and forest (or re-forested area), the length of the ELS ⁶ Lip can be established by computing a weighted average of the lengths required for each vegetation type. Refer to **Section 6.3** for design criteria

⁵ The plan approving authority may waive the requirement for compost amended soils for filter strips on B soils under certain conditions (see **Section 6.1**).

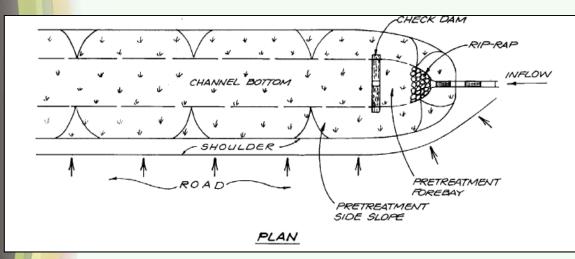
^b ELS = Engineered Level Spreader; GD = Gravel Diaphragm; PB = Permeable Berm.

Specification No. 3: Grass Channels

What is it?

Grass-lined conveyance channels to treat runoff from:

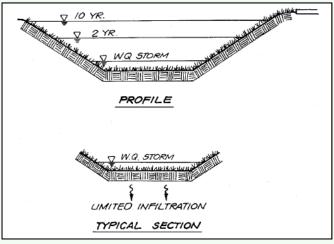
- Highways;
- Low- to medium-density residential yards;
- Driveways;
- Ball fields; and
- Small commercial parking areas.



Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
	1	10 to 20	20	50 to 75	15	24 to 41
Grass Channels			No Leve	l 2 Design		



Grass Channel Source: DCR Stormwater Design Spec No. 3



Grass channel, typical plan and section views DCR Stormwater Design Spec No. 3

Specification No. 3: Grass Channels (cont.)

Stormwater Functions Summary

Table 3.1. Summar	ry of Stormwater Functions Provided by Grass Channels ¹
, and a diff a difficulty	

Stormwater Function	HSG Soi	Is A and B	HSG So	HSG Soils C and D		
Stormwater Function	No CA 2	With CA	No CA	With CA		
Annual Runoff Volume Reduction (RR)	20%	NA ³	10%	30%		
Total Phosphorus (TP) EMC Reduction ⁴ by BMP Treatment Process	1	5%	1	15%		
Total Phosphorus (TP) Mass Load Removal	3	2%		no CA) to with CA)		
Total Nitrogen (TN) EMC Reduction ⁴ by BMP Treatment Process	2	0%	2	20%		
Total Nitrogen (TN) Mass Load Removal	3	6%	28% (no CA) to 44% (with CA)			
Channel & Flood Protection	adjust curve contributing reduction ac path should	e number for drainage area hieved. Also, th	use the RRM spreadsheet to for each design storm for the area, based on annual runoff the Tc for the grass swale flow slope and appropriate roughness we cover.			

CWP and CSN (2008) and CWP (2007).

⁴ Change in event mean concentration (EMC) through the practice. Actual nutrient mass load removed is the product of the pollutant removal rate and the runoff volume reduction rate (see Table 1 in the *Introduction to the New Virginia Stormwater Design Specifications*).

Design Criteria

Table 3.2. Grass Channel Design Guidance

Design Criteria

The bottom width of the channel should be between 4 to 8 feet wide.

The channel side-slopes should be 3H:1V or flatter.

The maximum total contributing drainage area to any individual grass channel is 5 acres.

The longitudinal slope of the channel should be no greater than 4%. (Check dams may be used to reduce the effective slope in order to meet the limiting velocity requirements.)

The maximum flow velocity of the channel must be less than 1 foot per second during a 1-inch storm event

The dimensions of the channel should ensure that flow velocity is non-erosive during the 2-year and 10-year design storm events and the 10-year design flow is contained within the channel (minimum of 6 inches of freeboard).

² CA= Compost Amended Soils, see Stormwater Design Specification No. 4.

³ Compost amendments are generally not applicable for A and B soils, although it may be advisable to incorporate them on mass-graded and/or excavated soils to maintain runoff reduction rates. In these cases, the 30% runoff reduction rate may be claimed, regardless of the pre-construction HSG.

Specification No. 4: Soil Compost Amendment

What is it?

Soil may be amended with compost to:

- Reduce runoff from compacted lawns;
- Enhance rooftop disconnections;
- Enhance grass channels;
- Enhance vegetated filter strips; and
- Enhance reforestation areas.

Amendment is not recommended when:

- Existing soils have high infiltration rates;
- The water table or bedrock is within 1.5' of the soil surface;
- Existing soils are saturated or seasonally wet;
- Amendments would harm the roots of existing trees;
- The downhill slope runs toward a foundation; or
- The contributing impervious surface is larger than the surface area of the amended soils.



Soil compost amendment Source: DCR Stormwater Design Spec No. 4

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Soil Compost Amendment	See t	used to decreathe design special	ecs for Rooft	op Disconne	ction, Sheet	Flow to

Specification No. 4: Soil Compost Amendment (cont.)

Stormwater Functions Summary

Table 4.1: Stormwater Functions of Soil Compost Amendments 1

Stormwater Function	HSG Soi	Is A and B	HSG Soi	Is C and D
Stormwater Function	No CA 2	With CA	No CA	With CA
Annual Runoff Volume Reduction (RR)				
Simple Rooftop Disconnection	50%	NA ³	25%	50%
Filter Strip	50%	NA 3	NA ⁴	50%
Grass Channel	20%	NA ³	10%	30%
Total Phosphorus (TP) EMC				•
Reduction ⁴ by BMP Treatment	0		0	
Practice				
Total Phosphorus (TP) Mass Load Removal	Same as for RR (above)		Same as fo	r RR (above)
Total Nitrogen (TN) EMC Reduction by BMP Treatment Practice	0		0	
Total Nitrogen (TN) Mass Load Removal	Same as fo	r RR (above)	Same as fo	r RR (above)
Channel Protection & Flood Mitigation	adjust the contributing	igners can use urve number for drainage area, stion achieved.	each design	storm for the

¹ CWP and CSN (2008), CWP (2007)

Runoff Coefficients

Table 4.2. Runoff Coefficients for Use for Different Pervious Areas

Hydrologic Soil Group	Undisturbed Soils ¹	Disturbed Soils ²	Restored and Reforested ³
Α	0.02	0.15	0.02
В	0.03	0.20	0.03
С	0.04	0.22	0.04
D	0.05	0.25	0.05

Notes:

¹ Portions of a new development site, outside the limits of disturbance, which are not graded and do not receive construction traffic.

² Previously developed sites, and any site area inside the limits of disturbance as shown on the E&S Control plan.

Compost Depths

Table 4.3. Short-Cut Method to Determine Compost and Incorporation Depths

	Contributing Impervious Cover to Soil Amendment Area Ratio ¹					
	IC/SA = 0 ²	IC/SA = 0.5	IC/SA = 0.75	IC/SA = 1.0 3		
Compost (in) 4	2 to 4 5	3 to 6 5	4 to 8 ⁵	6 to 10 ⁵		
Incorporation Depth (in)	6 to 10 ⁵	8 to 12 ⁵	15 to 18 ⁵	18 to 24 ⁵		
Incorporation Method	Rototiller Tiller Subsoiler Subsoiler					

Notes

- ¹ IC = contrib. impervious cover (sq. ft.) and SA = surface area of compost amendment (sq. ft.)
- ² For amendment of compacted lawns that do not receive off-site runoff
- In general, IC/SA ratios greater than 1 should be avoided
- ⁴ Average depth of compost added
- Lower end for B soils, higher end for C/D soils

² CA = Compost Amended Soils, see Stormwater Design Specification No. 4.

³ Compost amendments are generally not applicable for A and B soils, although it may be advisable to incorporate them on mass-graded B soils to maintain runoff reduction rates.

⁴ Filter strips in HSG C and D should use composted amended soils to enhance runoff reduction capabilities. See Stormwater Design Specification No. 2: Sheetflow to Vegetated Filter Strip or Conserved Open Space.

³ Areas with restored soils that are also reforested to achieve a minimum 75% forest canopy

Specification No. 5: Vegetated Roof

What is it?

A rooftop covered with soil media and plants. May be:

- Extensive with shallow soil and a limited plant palette; or
- Intensive with deep soil and a wide plant palette.

Vegetated roofs are recommended for non-residential, multi-family, and mixed-use buildings.



Green roof at WSSI
Source: Wetland Studies and Solutions, Inc.



Green roof at Fairfax County Government Center parking structure Source: http://www.fairfaxcounty.gov/news/images/roof_garden_.jpg

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Vagatated Boof	1	45	0	45	0	45
Vegetated Roof	2	60	0	60	0	60

Specification No. 5: Vegetated Roof (cont.)

Stormwater Functions Summary

Table 5.1: Summary of Stormwater Functions Provided by Vegetated Roofs 1

Stormwater Function	Level 1 Design	Level 2 Design		
Annual Runoff Volume Reduction (RR)	45%	60%		
Total Phosphorus (TP) EMC				
Reduction by BMP Treatment	0	0		
Process				
Total Phosphorus (TP) Mass Load	45%	60%		
Removal	40 70	00 70		
Total Nitrogen (TN) EMC				
Reduction ² by BMP Treatment	0	0		
Process				
Total Nitrogen (TN) Mass Load	45%	60%		
Removal	45 %	00 76		
Channel Protection & Flood Mitigation ³	Use the following Curve Numbers (CN) for Design Storm ever 1-year storm = 64; 2-year storm = 66; 10-year storm = 72; the 100 year storm = 75			

¹ Sources: CWP and CSN (2008) and CWP (2007).

² Moran et al (2004) and Clark et al (2008) indicate no nutrient reduction or even negative nutrient reduction (due to leaching from the media) in early stages of vegetated roof development.





Design Criteria

Table 5.2. Green Roof Design Guidance					
Level 1 Design (RR:45; TP:0; TN:0)	Level 2 Design (RR: 60; TP:0; TN:0)				
$Tv = 1.0 (Rv)^{1} (A)/12$	$Tv = 1.1 (Rv)^{1} (A)/12$				
Depth of media up to 4 inches	Media depth 4 to 8 inches				
Drainage mats 2-inch stone drainage layer					
No more than 20% organic matter in media No more than 10% organic matter in media					
All Designs: Must be in conformance to ASTM (2005) International Green (Vegetated) Roof Stds.					
Rv represents the runoff coefficient for a conventional roof, which will usually be 0.95. The runoff reduction rate applied to the vegetated roof is for "capturing" the Treatment Volume (Tv) compared to what a conventional roof would produce as runoff.					

Material Specifications

Table 5.4. Extensive Vegetated Roof Material Specifications					
Material	Specification				
Roof	Structural Capacity should conform to ASTM E-2397-05, Practice for Determination of Live Loads and Dead Loads Associated with Green (Vegetated) Roof Systems. In addition, use standard test methods ASTM E2398-05 for Water Capture and Media Retention of Geocomposite Drain Layers for Green (Vegetated) Roof Systems, and ASTME 2399-05 for Maximum Media Density for Dead Load Analysis.				
Waterproof Membrane	See Chapter 6 of Weiler and Scholz-Barth (2009) for waterproofing options that are designed to convey water horizontally across the roof surface to drains or gutter. This layer may sometimes act as a root barrier.				
Root Barrier	Impermeable liner that impedes root penetration of the membrane.				
Drainage Layer	1 to 2 inch layer of clean, washed granular material, such as ASTM D 448 size No. 8 stone. Roof drains and emergency overflow should be designed in accordance with VUSBC.				
Filter Fabric	Needled, non-woven, polypropylene geotextile. Density (ASTM D3776) > 16 oz./sq. yd., or approved equivalent. Puncture resistance (ASTM D4833) > 220 lbs., or approved equivalent.				
Growth Media	80% lightweight inorganic materials and 20% organic matter (e.g. well-aged compost). Media should have a maximum water retention capacity of around 30%. Media should provide sufficient nutrients and water holding capacity to support the proposed plant materials. Determine acceptable saturated water permeability using ASTM E2396-05.				
Plant Materials	Sedum, herbaceous plants, and perennial grasses that are shallow-rooted, self-sustaining, and tolerant of direct sunlight, drought, wind, and frost. See ASTM E2400-06, Guide for Selection, Installation and Maintenance of Plants for Green (Vegetated) Roof Systems.				

Green roof at Sidwell Friends School

Specification No. 6: Rainwater Harvesting

What is it?

Capturing roof runoff for non-potable interior and exterior uses. Note that:

- Credit is only given for dedicated year-round drawdown for the water.
- Irrigation will not receive credit without a secondary practice to treat water during the winter.
- A Virginia-specific amendment to the 2009 Uniform Statewide Building Code limits harvested water storage to 24 hours for irrigation and 72 hours for flushing water closets and urinals.



Underground rainwater harvesting cistern Source: DCR Stormwater Design Spec No. 6

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Rainwater Harvesting	1	Up to 90	0	Up to 90	0	Up to 90
	No Level 2 Design					



Above-ground rainwater harvesting cistern at WSSI Source: Wetland Studies and Solutions, Inc.

Specification No. 6: Rainwater Harvesting (cont.)

Stormwater Functions Summary

Table 6.1: Summary of Stormwater Functions Provided by Rainwater Harvesting

Stormwater Function	Performance
Annual Runoff Volume Reduction (RR)	Variable up to 90% ²
Total Phosphorus (TN) EMC Reduction ¹ by BMP Treatment Process	0%
Total Phosphorus (TN) Mass Load Removal	Variable up to 90% ²
Total Nitrogen (TN) EMC Reduction ¹ by BMP Treatment Process	0%
Total Nitrogen (TN) Mass Load Removal	Variable up to 90% ²
Channel Protection	Partial: reduced curve numbers and increased Time of Concentration
Flood Mitigation	Partial: reduced curve numbers and increased Time of Concentration

¹ Nutrient mass removal is equal to the runoff reduction rate. Zero additional removal rate is applied to the rainwater harvesting system only. Nutrient removal rates for secondary practices will be in accordance with the design criteria for those practice.

Material Considerations

Table 6.2. Advantages and Disadvantages of Various Cistern Materials						
Tank Material	Advantages	Disadvantages				
Fiberglass	Commercially available, alterable and moveable; durable with little maintenance; light weight; integral fittings (no leaks); broad application	Must be installed on smooth, solid, level footing; pressure proof for below-ground installation; expensive in smaller sizes				
Polyethylene	Commercially available, alterable, moveable, affordable; available in wide range of sizes; can install above or below ground; little maintenance; broad application Can be UV-degradable; must painted or tinted for above-ground installations; pressure-proof for be ground installation					
Modular Storage	Can modify to topography; can alter footprint and create various shapes to fit site; relatively inexpensive Longevity may be less than materials; higher risk of punctur water tight membrane construction					
Plastic Barrels	Commercially available; inexpensive	Low storage capacity (20 to 50 gallons); limited application				
Galvanized Steel	Commercially available, alterable and moveable; available in a range of sizes; film develops inside to prevent corrosion	Possible external corrosion and rust; must be lined for potable use; can only install above ground; soil pH may limit underground applications				
Steel Drums	Commercially available, alterable and moveable	Small storage capacity; prone to corrosion, and rust can lead to leaching of metals; verify prior to reuse for toxics; water pH and soil pH may also limit applications				
FerroConcrete	Durable and immoveable; suitable for above or below ground installations; neutralizes acid rain	Potential to crack and leak; expensive				
Cast in Place Concrete	Durable, immoveable, versatile; suitable for above or below ground installations; neutralizes acid rain	Potential to crack and leak; permanent; will need to provide adequate platform and design for placement in clay soils				
Stone or concrete Block	Stone or concrete Durable and immoveable; keeps Difficult to maintain; expensive to build					
Source. Cabell Diditio, 2007, 2009						

² Credit is variable and determined using the Cistern Design Spreadsheet. Credit up to 90% is possible if all water from storms with rainfall of 1 inch or less is used through demand, and the tank is sized such that no overflow from this size event occurs. The total credit may not exceed 90%.

Specification No. 7: Permeable Pavement

What is it?

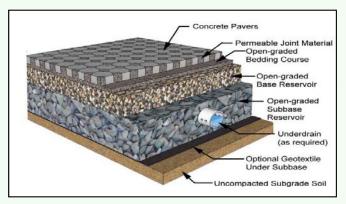
Alternative paving surface that allows water to filter through a permeable top layer into a gravel reservoir for temporary storage and/or infiltration. May replace impervious surfaces

on commercial, institutional, and residential sites.



Permeable pavers (brick) at the Virginia Capitol Building Source: Wetland Studies and Solutions, Inc.

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Permeable	1	45	25	59	25	59
Pavement	2	75	25	81	25	81



Typical permeable paver section DCR Stormwater Design Spec No. 7



Permeable pavers (concrete) at WSSI Source: Wetland Studies and Solutions, Inc.

Specification No. 7: Permeable Pavement (cont.)

Stormwater Functions Summary

Table 7.1. Summary of Stormwater Functions Provided by Permeable Pavement

Stormwater Function	Level 1 Design	Level 2 Design	
Annual Runoff Volume Reduction (RR)	45%	75%	
Total Phosphorus (TP) EMC Reduction ¹ by BMP Treatment Process	25%	25%	
Total Phosphorus (TP) Mass Load Removal	59%	81%	
Total Nitrogen (TN) EMC Reduction ¹	25%	25%	
Total Nitrogen (TN) Mass Load Removal	59%	81%	
Channel Protection	storm volumes, and us Equations ² to compute	nt; OR otional, as needed) in the to accommodate larger se NRCS TR-55 Runoff a CN adjustment.	
Partial. May be able to design additional s into the reservoir layer by adding perforate storage pipe or chambers.			

¹ Change in event mean concentration (EMC) through the practice. Actual nutrient mass load removed is the product of the removal rate and the runoff reduction rate (see Table 1 in the *Introduction to the New Virginia Stormwater Design Specifications*).

Design Criteria

Table 7.3. Permeable Pavement Design Criteria

Level 1 Design	Level 2 Design		
Tv = $(1)(Rv)(A) / 12$ – the volume reduced by an upstream BMP ¹	Tv = (1.1)(Rv)(A) / 12		
Soil infiltration is less than 0.5 in./hr.	Soil infiltration rate exceeds 0.5 in./hr.		
Underdrain required	Underdrain not required; <i>OR</i> If an underdrain is used, a 12-inch stone sump must be provided below the underdrain invert; <i>OR</i> The Tv has at least a 48-hour drain time, as regulated by a control structure.		
CDA = The permeable pavement area plus upgradient parking, as long as the ratio of external contributing area to permeable pavement does not exceed 2:1.	CDA = The permeable pavement area		

The contributing drainage area to the permeable pavements should be limited to paved surfaces, to avoid sediment wash-on, and sediment source controls and/or a pre-treatment strip or sump should be used. When pervious areas are conveyed to permeable pavement, pre-treatment must be provided, and the pre-treatment may qualify for a runoff reduction credit.

Material Specifications

Design Factor	Porous Concrete (PC)	Porous Asphalt (PA)	Interlocking Pavers (IP)	
Scale of Application	Small and large scale paving applications	Small and large scale paving applications	Micro, small and large scale paving applications	
Pavement Thickness 1	5 to 8 inches	3 to 4 inches	3 inches 1, 8	
Bedding Layer 1,8	None	2 inches No. 57 stone	2 inches of No. 8 stone	
Reservoir Layer ^{2, 8}	No. 57 stone	No. 2 stone	No. 2 stone 3-4 inches of No.57 stone	
Construction Properties Cast in place, seven day cure, must be covered Cast in place, 24 hour cure		to the second se	No cure period; manual or mechanical installation of pre-manufactured units, ove 5000 st/day per machine	
Design Permeability 4	10 feet/day	6 feet/day	2 feet/day	
Construction Cost 5 \$ 2.00 to \$6.50/sq. ft.		\$ 0.50 to \$1.00/ sq. ft.	\$ 5.00 to \$ 10.00/ sq. ft.	
Min. Batch Size	500 s	q. ft.	NA	
Longevity ⁶	20 to 30 years	15 to 20 years	20 to 30 years	
Overflow	Drop inlet or overflow edge	Drop inlet or overflow edge	Surface, drop inlet or overflow edge	
Temperature Reduction	Cooling in the reservoir layer	Cooling in the reservoir layer	Cooling at the pavement surface & reservoir layer	
Colors/Texture	Limited range of colors and textures	Black or dark grey color	Wide range of colors, textures, and patterns	
Traffic Bearing Capacity ⁷	Can handle all traffic loads, with appropriate bedding layer design.			
Surface Clogging	Replace paved areas or install drop inlet	Replace paved areas or install drop inlet	Replace permeable stone jointing materials	
Other Issues		Avoid seal coating	Snowplow damage	
Design Reference American Concrete Institute # 522.1.08		Jackson (2007) NAPA	Smith (2006) ICPI	

¹ Individual designs may depart from these typical cross-sections, due to site, traffic and design conditions.

² NRCS TR-55 Runoff Equations 2-1 thru 2-5 and Figure 2-1 can be used to compute a curve number adjustment for larger storm events based on the retention storage provided by the practice(s).
Sources: CWP and CSN (2008) and CWP (2007)

Reservoir storage may be augmented by corrugated metal pipes, plastic arch pipe, or plastic lattice blocks.
3 ICPI (2008)

^{4.000}

⁴NVRA (2008)

⁵ WERF 2005 as updated by NVRA (2008)

⁶ Based on pavement being maintained properly, Resurfacing or rehabilitation may be needed after the indicated period.

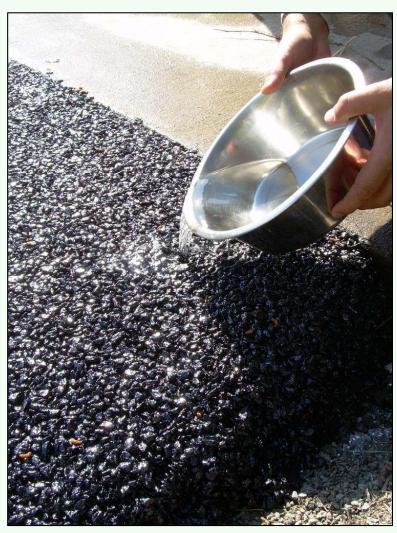
Depends primarily on on-site geotechnical considerations and structural design computations.

⁸ Stone sizes correspond to ASTM D 448: Standard Classification for Sizes of Aggregate for Road and Bridge Construction.

Specification No. 7: Permeable Pavement (cont.)



Pervious Concrete at WSSI



Porous Asphalt at WSSI

Specification No. 8: Infiltration Practices

What is it?

Temporary surface or below-grade storage to detain and infiltrate runoff into the in-situ soil.

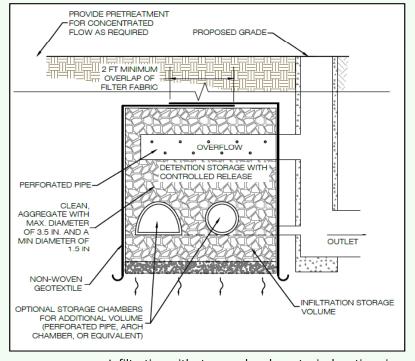
Has the greatest runoff reduction potential of all BMPs, but measured infiltration rates must be greater than 0.5 inches per hour.



Infiltration trench

Source: DCR Stormwater Design Spec No. 8

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Infiltration	1	50	15	57	25	63
Practices	2	90	15	92	25	93



Infiltration with storage chambers, typical section view DCR Stormwater Design Spec No. 8

Specification No. 8: Infiltration Practices (cont.)

ON TOP OF PEA GRAVEL INFLOW PRETREATMENT AS REQUIRED PEA GRAVEL OR RIVER STONE OUTLET TO STORM SEWER OR **OVERFLOW** DAYLIGHT OUTFALL CLEAN, AGGREGATE WITH MAX. DIAMETER OF 3.5 IN. AND A MIN DIAMETER OF SAND FILTER 6" DEEP (OR FABRIC EQUIVALENT) OBSERVATION WELL SLOPES CONSISTENT WITH-PRETREATMENT PEA GRAVEL OR RIVER STONE NON-WOVEN CLEAN, AGGREGATE WITH MAX. DIAMETER OF 3.5 IN. AND A MIN DIAMETER OF 1.5 IN SAND FILTER 6 - 8" DEEP (OR FABRIC EQUIVALENT)

Infiltration trench typical profile and section views DCR Stormwater Design Spec No. 8

*Note that this design specification does not define a maximum allowable infiltration rate, but the VSMH requires an infiltration rate between 0.52 and 8.27 in/hr. (See VSMH Standard 3.10.)

Stormwater Functions Summary

Stormwater Function	Level 1 Design	Level 2 Design		
Annual Runoff Volume Reduction (RR)	50%	90%		
Total Phosphorus (TP) EMC Reduction ¹ by BMP Treatment Process	25%	25%		
Total Phosphorus (TP) Mass Load Removal	63%	93%		
Total Nitrogen (TN) EMC Reduction ¹ by BMP Treatment Process	15%	15%		
Total Nitrogen (TN) Mass Load Removal	57%	92%		
Channel and Flood Protection	Use the RRM spreadsheet to calculate the Curve Number (CN) adjustment; OR Design for extra storage (optional; as needed) on the surface or in the subsurface storage volume to accommodate larger storm volumes, and use NRCS TR-55 Runoff Equations 2 to compute the CN Adjustment.			

Introduction to the New Virginia Stormwater Design Specifications).

² NRCS TR-55 Runoff Equations 2-1 thru 2-5 and Figure 2-1 can be used to compute a curve number adjustment for larger storm events, based on the retention storage provided by the practice(s)

Sources: CWP and CSN (2008), and CWP (2007)

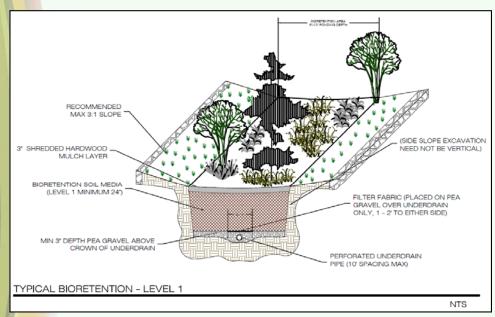
Design Criteria

Table 8.2. Level 1 and Level 2 Infiltration Design Guidelines				
Level 1 Design (RR:50; TP:25; TN:15)	Level 2 Design (RR:90; TP:25; TN:15)			
Sizing: T _v = [(Rv)(A)/12] – the volume reduced by an upstream BMP	Sizing: T _v = [1.1(Rv)(A)/12] – the volume reduced by an upstream BMP			
At least two forms of pre-treatment (see Table 8.6) At least three forms of pre-treatment (see Table 8.6)				
Soil infiltration rate 1/2 to 1 in./hr. (see Section 6.1 & Appendix 8-A); number of tests depends on the scale (Table 3) Soil infiltration rates of 1.0 to 4.0 in/hr (see Section 6.1 & Appendix 8-A); number of tests depends on the scale (Table 8.3)				
Minimum of 2 feet between the bottom of the infiltration practice and the seasonal high water table or bedrock (Section 4.5)				
T _v infiltrates within 36 to 48 hours (Section 6.6)				
Building Setbacks – see Table 8.3				
All Designs are subject to hotsp	oot runoff restrictions/prohibitions			

Specification No. 9: Bioretention Practices

What is it?

Shallow, depressed landscape feature that collects runoff and filters it through a sandy, engineered soil media. Bioretention provides evapotranspiration, infiltration, and storage.



Bioretention typical section view

DCR Stormwater Design Spec No. 9

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Bioretention	1	40	40	64	25	55
Practices	2	80	60	90	50	90



Bioretention at WSSI Source: Wetland Studies and Solutions, Inc.

Specification No. 9: Bioretention Practices (cont.)

Stormwater Functions Summary

Table 9.1. Summary of Stormwater Functions Provided by Bioretention Basins

Stormwater Function	Level 1 Design	Level 2 Design	
Annual Runoff Volume Reduction (RR)	40%	80%	
Total Phosphorus (TP) EMC Reduction ¹ by BMP Treatment Process	25%	50%	
Total Phosphorus (TP) Mass Load Removal	55%	90%	
Total Nitrogen (TN) EMC Reduction ¹ by BMP Treatment Process	40%	60%	
Total Nitrogen (TN) Mass Load Removal	64% 90%		
Channel and Flood Protection	Use the Runoff Reduction Method (RRM) Spreadsheet to calculate the Cover Number (CN) Adjustment OR Design extra storage (optional; as needed) on the surface, the engineered soil matrix, and in the stone/underdrain layer to accommodate a larger storm, and use NRCS TR-55 Run		

¹ Change in event mean concentration (EMC) through the practice. Actual nutrient mass load removed is the product of the removal rate and the runoff reduction rate(see Table 1 in the *Introduction to the New Virginia Stormwater Design Specifications*).

Equations² to compute the CN Adjustment.

Sources: CWP and CSN (2008) and CWP (2007)

Material Considerations

Table 9.6. Bioretention Material Specifications				
Material	Specification	Notes		
Filter Media Composition	Filter Media to contain: 85%-88% sand 8%-12% soil fines 3%-5% organic matter in the form of leaf compost	The volume of filter media based on 110% of the plan volume, to account for settling or compaction.		
Filter Media Testing	P-Index range = 10-30, OR Between 7 and 21 mg/kg of P in the soil media. CECs greater than 10	The media must be procured from approved filter media vendors.		
Mulch Layer	Use aged, shredded hardwood bark mulch	Lay a 2 to 3 inch layer on the surface of the filter bed.		
Alternative Surface Cover	Use river stone or pea gravel, coir and jute matting, or turf cover.	Lay a 2 to 3 inch layer of to suppress weed growth.		
Top Soil For Turf Cover	Loamy sand or sandy loam texture, with less than 5% clay content, pH corrected to between 6 and 7, and an organic matter content of at least 2%.	3 inch surface depth.		
Geotextile/Liner	Use a non-woven geotextile fabric with a flow rate of > 110 gal./min./sq. ft. (e.g., Geotex 351 or equivalent)	Apply only to the sides and above the underdrain. For hotspots and certain karst sites only, use an appropriate liner on bottom.		
Choking Layer	Lay a 2 to 4 inch layer of sand over a #89 washed gravel), which is laid over the	2 inch layer of choker stone (typically #8 or ne underdrain stone.		
Stone Jacket for Underdrain and/or Storage Layer	1 inch stone should be double-washed and clean and free of all fines (e.g., VDOT #57 stone).	12 inches for the underdrain; 12 to 18 inches for the stone storage layer, if needed		
Underdrains, Cleanouts, and Observation Wells	Use 6 inch rigid schedule 40 PVC pipe (or equivalent corrugated HDPE for micro-bioretention), with 3/8-inch perforations at 6 inches on center; position each underdrain on a 1% or 2% slope located nor more than 20 feet from the next pipe.	Lay the perforated pipe under the length of the bioretention cell, and install non-perforated pipe as needed to connect with the storm drain system. Install T's and Y's as needed, depending on the underdrain configuration. Extend cleanout pipes to the surface with vented caps at the Ts and Ys.		
Plant Materials	Plant one tree per 250 square feet (15 feet on-center, minimum 1 inch caliper). Shrubs a minimum of 30 inches high planted a minimum of 10 feet oncenter. Plant ground cover plugs at 12 to 18 inches on-center; Plant containergrown plants at 18 to 24 inches oncenter, depending on the initial plant size and how large it will grow.	Establish plant materials as specified in the landscaping plan and the recommended plant list. In general, plant spacing must be sufficient to ensure the plant material achieves 80% cover in the proposed planting areas within a 3-year period. If seed mixes are used, they should be from a qualified supplier, should be appropriate for stormwater basin applications, and should consist of native species (unless the seeding is to establish maintained turf).		

²NRCS TR-55 Runoff Equations 2-1 thru 2-5 and Figure 2-1 can be used to compute a curve number adjustment for larger storm events based on the retention storage provided by the practice(s).

Specification No. 9: Bioretention Practices (cont.)

DCR Specification No. 9 Design Criteria

Table 9.2. Micro-Bioretention (Rain Garden) Design Criteria

Level 1 Design (RR 40 TP: 25)	Level 2 Design (RR: 80 TP: 50)			
Sizing: Filter surface area (sq. ft.) = 3% ² of the contributing drainage area (CDA).	Sizing: Filter surface area (sq. ft.) = 4% ² of the CDA (can be divided into different cells at downspouts).			
Maximum contributing drainage area =	0.5 acres; 25% Impervious Cover (IC) 2			
One cell design (can be divided into s	smaller cells at downspout locations) 2			
	Depth = 6 inches			
Filter Media Depth minimum = 18 inches; Recommended maximum = 36 inches	Filter Media Depth minimum = 24 inches; Recommended maximum = 36 inches			
Media: mixed on-site or supplied by vendor	Media: supplied by vendor			
All Designs: Media mix tested for an acceptable phosphorus index				
(P-Index) of between 10 and 30, OR				
Between 7 and 21 mg/l-	kg of P in the soil media			
Sub-soil testing: not needed if an underdrain is used; Min infiltration rate > 1 inch/hour in order to remove the underdrain requirement.	<u>Sub-soil testing</u> : one per practice; Min infiltration rate > 1/2 inch/hour; Min infiltration rate > 1 inch/hour in order to remove the underdrain requirement.			
<u>Underdrain</u> : corrugated HDPE or equivalent.	<u>Underdrain</u> : corrugated HDPE or equivalent, with a minimum 6-inch stone sump below the invert; OR none, if soil infiltration requirements are met			
<u>Clean-outs</u> :	not needed			
Inflow: sheetfloom	w or roof leader			
<u>Pretreatment</u> : external (leaf screens, grass filter strip, energy dissipater, etc.).	Pretreatment: external plus a grass filter strip			
Vegetation: turf, herbaceous, or shrubs (min = 1 out of those 3 choices).	<u>Vegetation</u> : turf, herbaceous, shrubs, or trees (min = 2 out of those 4 choices).			
Building setbacks: 10 feet dow	n-gradient; 25 feet up-gradient			

Consult Appendix 9-A for design criteria for Urban Bioretention Practices.

² Micro-Bioretention (Rain Gardens) can be located at individual downspout locations to treat up to 1,000 sq. ft. of impervious cover (100% IC); the surface area is sized as 5% of the roof area (Level 1) or 6% of the roof area (Level 2), with the remaining Level 1 and Level 2 design criteria as provided in Table 9.2. If the Rain Garden is located so as to capture multiple rooftops, driveways, and adjacent pervious areas, the sizing rules within Table 9.2 should apply.

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Bioretention	1	40	40	64	25	55
Practices	2	80	60	90	50	90

T-61-00	Bioretention	Filher and	Danie.	Danier	Ouitania
rapie 9.3.	Bioretention	Filter and	Basin	vesian	Criteria

Table 9.3. Bioretention Filter and Basin Design Criteria				
Level 1 Design (RR 40 TP: 25)	Level 2 Design (RR: 80 TP: 50)			
Sizing (Section 6.1):	Sizing (Section 6.1):			
Surface Area (sq. ft.) = $(T_v - the volume reduced)$	Surface Area (sq. ft.) = [(1.25)(T _v) - the volume			
by an upstream BMP) / Storage Depth 1	reduced by an upstream BMP] /Storage Depth 1			
	buting drainage area = 2.5 acres			
	aximum Ponding Depth = 6 to 12 inches 2			
Filter Media Depth minimum = 24 inches;	Filter Media Depth minimum = 36 inches;			
recommended maximum = 6 feet	recommended maximum = 6 feet			
	by vendor; tested for acceptable phosphorus index			
	een 10 and 30, <i>OR</i>			
	kg of P in the soil media Sub-soil Testing (Section 6.2); one per 1,000 sq.			
	ft. of filter surface; Min infiltration rate > 1/2			
	inch/hour in order to remove the underdrain			
requirement.	requirement.			
	Underdrain & Underground Storage Layer			
Underdrain (Section 6.7) = Schedule 40 PVC with	(Section 6.7) = Schedule 40 PVC with clean outs,			
clean-outs	and a minimum 12-inch stone sump below the			
olour out	invert; OR, none, if soil infiltration requirements			
Inflant shootflest such sute transh dra	are met (Section 6.2)			
Geometry (Section 6.3):	ns, concentrated flow, or the equivalent Geometry (Section 6.3):			
Length of shortest flow path/Overall length = 0.3;	Length of shortest flow path/Overall length = 0.8;			
OR , other design methods used to prevent short-	OR , other design methods used to prevent short-			
circuiting; a one-cell design (not including the pre-	circuiting; a two-cell design (not including the			
treatment cell).	pretreatment cell).			
Pre-treatment (Section 6.4): a pretreatment cell,	Pre-treatment (Section 6.4): a pretreatment cell			
grass filter strip, gravel diaphragm, gravel flow	plus one of the following: a grass filter strip, gravel			
spreader, or another approved (manufactured)	diaphragm, gravel flow spreader, or another			
pre-treatment structure.	approved (manufactured) pre-treatment structure.			
Conveyance & Overflow (Section 6.5)	Conveyance & Overflow (Section 6.5)			
Planting Plan (Section 6.8): a planting template to	Planting Plan (Section 6.8): a planting template to include turf, herbaceous vegetation, shrubs,			
include turf, herbaceous vegetation, shrubs,	and/or trees to achieve surface area coverage of			
and/or trees to achieve surface area coverage of	at least 90% within 2 years. If using turf, must			
at least 75% within 2 years.	combine with other types of vegetation 1.			
Building Sothan				
Building Setbacks ³ (Section 5):				

0 to 0.5 acre CDA = 10 feet if down-gradient from building or level (coastal plain); 50 feet if up-gradient. 0.5 to 2.5 acre CDA = 25 feet if down-gradient from building or level (coastal plain); 100 feet if up-gradient. (Refer to additional setback criteria in **Section 5**)

Deeded Maintenance O&M Plan (Section 8)

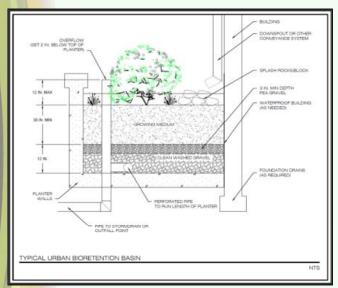
- ¹ Storage depth is the sum of the Void Ratio (V_t) of the soil media and gravel layers multiplied by their respective depths, plus the surface ponding depth. Refer to **Section 6.1**.
- A ponding depth of 6 inches is preferred. Ponding depths greater than 6 inches will require a specific planting plan to ensure appropriate plant selection (Section 6.8).
- ³ These are recommendations for simple building foundations. If an in-ground basement or other special conditions exist, the design should be reviewed by a licensed engineer. Also, a special footing or drainage design may be used to justify a reduction of the setbacks noted above.

Specification No. 9A: Urban Bioretention

What is it?

Bioretention adapted to the ultra-urban climate, including:

- Stormwater planters;
- Extended tree pits; and
- Stormwater curb extensions



Stormwater planter typical section view DCR Stormwater Design Spec No. 9A

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Urban	1	40	40	64	25	55
Bioretention	No Level 2 Design					·

DCR Specification No. 10 Design Criteria

Table 9-A.2. Urban Bioretention Design Criteria

Level 1 Design Only (RR: 40; TP: 25)

Sizing (Refer to Section 9-A-6.1):

Surface Area (sq. ft.) = $T_v/2 = \{[(1.0 \text{ inch})(R_v)(A)/12)]$ – the volume reduced by an upstream BMP}/2

Underdrain = Schedule 40 PVC with clean-outs

(Refer to the Main Bioretention Design Specification, Section 9.8)

Maximum Drainage Area = 2,500 sq. ft.

Maximum Ponding Depth = 6 to 12 inches

Filter media depth minimum = 30 inches: recommended maximum = 48 inches

Media and Surface Cover (Refer to the Main Bioretention Design Specification, Section 9.8)

Sub-soil testing (Refer to the Main Bioretention Design Specification, Section 9.8)

Inflow = sheetflow, curb cuts, trench drains, roof drains, concentrated flow, or equivalent

Building setbacks (Refer to Section A-4 9-A-5)

Deeded maintenance O&M plan (Refer to the Main Bioretention Design Specification, Section 9.1)

Ponding depth above 6 inches will require a specific planting plan to ensure appropriate plants (Refer to the Main Bioretention Design Specification, **Section 6.8**).



Stormwater planter

Source: DCR Stormwater Design Spec No. 9A



Stormwater curb extension

Source: DCR Stormwater Design Spec No. 9A

Specification No. 9A: Urban Bioretention (cont.)

Stormwater Functions Summary

Table 9-A.1. Summary of Stormwater Functions Provided by Urban Bioretention Areas

Stormwater Function	Level 1 Design	Level 2 Design		
Annual Runoff Volume Reduction (RR)	40% (for Water Quality credit in the RRM spreadsheet only) 0% credit for Channel Protection	NA		
Total Phosphorus (TP) EMC Reduction ¹ by BMP Treatment Process	25%	NA		
Total Phosphorus (TP) Mass Load Removal	55%			
Total Nitrogen (TN) EMC Reduction by BMP Treatment Process	40%	NA		
	64%			
Channel Protection	None; or if sized according to Bio Level 1 Bioretention basin criteria.	pretention Basin, follow the		
Flood Mitigation	None			

Change in the event mean concentration (EMC) through the practice. The actual nutrient mass load removed is the product of the removal rate and the runoff reduction rate (see Table 1 in the *introduction to the New Virginia Stormwater Design Specifications*).

Sources: CWP and CSN (2008) and CWP (2007)



Urban bioretention in Richmond, VA
Source: Wetland Studies and Solutions. Inc.

Design Criteria

Table 9-A.2. Urban Bioretention Design Criteria

Urban bioretention in Washington, D.C.

Source: http://www.cenews.com/magazine-article-cenews.com-9-2009-civil_engineering_design__for_green_building-7592.html

Level 1 Design Only (RR: 40; TP: 25)

Sizing (Refer to Section 9-A-6.1):

Surface Area (sq. ft.) = $T_v/2 = \{[(1.0 \text{ inch})(R_v)(A)/12)]$ – the volume reduced by an upstream BMP}/2

Underdrain = Schedule 40 PVC with clean-outs

(Refer to the Main Bioretention Design Specification, Section 9.8)

Maximum Drainage Area = 2,500 sq. ft.

Maximum Ponding Depth = 6 to 12 inches 1

Filter media depth minimum = 30 inches: recommended maximum = 48 inches

Media and Surface Cover (Refer to the Main Bioretention Design Specification, **Section 9.8**)
Sub-soil testing (Refer to the Main Bioretention Design Specification, **Section 9.8**)

Inflow = sheetflow, curb cuts, trench drains, roof drains, concentrated flow, or equivalent

Building setbacks (Refer to Section A-4 9-A-5)

Deeded maintenance O&M plan (Refer to the Main Bioretention Design Specification, Section 9.1)

Ponding depth above 6 inches will require a specific planting plan to ensure appropriate plants (Refer to the Main Bioretention Design Specification, **Section 6.8**).

Specification No. 10: Dry Swales

What is it?

Shallow, linear, sloped bioretention that may be designed as:

- Conveyance swales to accept and convey sheet flow from linear watersheds such as roadways; or
- Treatment swales to accept and convey concentrated runoff from non-linear watersheds.

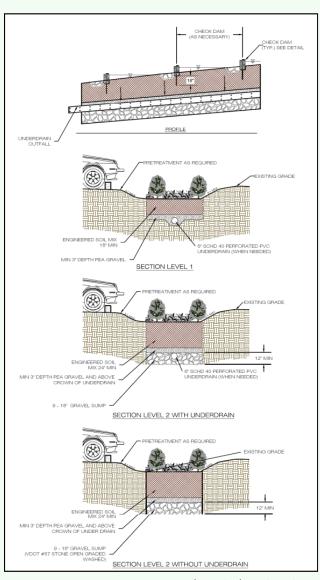
Dry swales differ from grass channels because they incorporate bioretention soil media.



Dry swale

Source: DCR Stormwater Design Spec No. 10

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Dry Swales	1	40	25	55	20	52
	2	60	35	74	40	76



Dry swale typical section views DCR Stormwater Design Spec No. 10

Specification No. 10: Dry Swales (cont.)

Stormwater Functions Summary

Table 10.1. Summary o	f Stormwater Functions Provide	ed by Dry Swales		
Stormwater Function	Level 1 Design	Level 2 Design		
Annual Runoff Volume Reduction (RR)	40%	60%		
Total Phosphorus (TP) EMC Reduction ¹ by BMP Treatment Process	20%	40%		
Total Phosphorus (TP) Mass Load Removal	52%	76%		
Total Nitrogen (TN) EMC Reduction ¹ by BMP Treatment Process	25%	35%		
Total Nitrogen (TN) Mass Load Removal	55%	74%		
Channel Protection	Use the RRM Design Spreadsheet to calculate the Cove Number (CN) Adjustment OR Design for extra storage (optional; as needed) on the surface in the engineered soil matrix, and in the stone/underdrail layer to accommodate a larger storm, and use NRCS TR-5 Runoff Equations ² to compute the CN Adjustment.			
Flood Mitigation	Partial. Reduced Curve Number			

Change in the event mean concentration (EMC) through the practice. The actual nutrient mass load removed is the product of the removal rate and the runoff reduction rate (see Table 1 in the Introduction to the New Virginia Stormwater Design Specifications).

NRCS TR-55 Runoff Equations 2-1 thru 2-5 and Figure 2-1 can be used to compute a curve number adjustment for larger storm events, based on the retention storage provided by the practice(s



Source: DCR Stormwater Design Spec No. 10

Design Criteria

Table 10.2. Dry Swale Design Criteria					
Level 1 Design (RR:40; TP:20; TN:25)	Level 2 Design (RR:60; TP:40; TN: 35)				
Sizing (Sec. 5.1):	Sizing (Sec. 5.1):				
Surface Area (sq. ft.) = (Tv- the volume reduced	Surface Area sq. ft.) = $\{(1.1)(T_v)$ - the volume				
by an upstream BMP) / Storage depth 1	reduced by an upstream BMP } / Storage Depth 1				
Effective swale slope ≤ 2%	Effective swale slope ≤ 1%				
Media Depth: minimum = 18 inches;	Media Depth minimum = 24 inches				
Recommended maximum = 36 inches	Recommended maximum = 36 inches				
Sub-soil testing (Section 6.2): not needed if an	Sub-soil testing (Section 6.2): one per 200 linear				
underdrain is used; min. infiltration rate must be >	feet of filter surface; min. infiltration rate must be				
1/2 inch/hour to remove the underdrain	> 1/2 inch/hour to remove the underdrain				
requirement;	requirement				
Underdrain (Section 6.7): Schedule 40 PVC with clean-outs	Underdrain and Underground Storage Layer (Section 6.7): Schedule 40 PVC with clean outs, and a minimum 12-inch stone sump below the invert; OR none if the soil infiltration requirements are met (see Section 6.2)				
Media (Section 6.6): supplied by the vendor	; tested for an acceptable phosphorus index:				
P-Index between 10 and 30; OR Betwee	n 7 and 23 mg/kg of P in the soil media 2				
Inflow: sheet or concentrated flo	w with appropriate pre-treatment				
	ll, grass filter strip, gravel diaphragm, gravel flow				
spreader, or another approved (manufactured) pre-treatment structure.					
On-line design	Off-line design or multiple treatment cells				
Turf cover	Turf cover, with trees and shrubs				
All Designs: acceptable media mix teste	d for phosphorus index (see Section 6.6)				



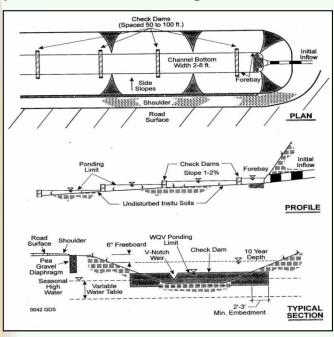
Source: http://www.publicbroadcasting.net/kunc/news. 62 newsmain?action=article&ARTICLE ID=1661510

Specification No. 11: Wet Swales

What is it?

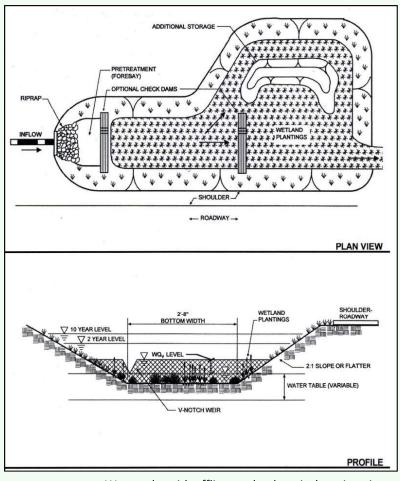
A hybrid between a swale and a wetland that is typically only recommended for flat coastal

plain locations with high water tables.



Wet swale typical section view DCR Stormwater Design Spec No. 11

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Wet Swales	1	0	25	25	20	20
	2	0	35	35	40	40



Wet swale with offline wetland, typical section view DCR Stormwater Design Spec No. 11

Specification No. 11: Wet Swales (cont.)

Design Criteria

Table 11.2. Wet Swale Design Criteria

Level 1 Design (RR:0; TP:20; TN:25)	Level 2 Design (RR:0; TP:40; TN:35)
$T_v = [(1 \text{ inch})(R_v)(A)] / 12 - \text{the volume reduced}$	$T_v = [(1.25 \text{ inch})(R_v)(A)] / 12 - \text{the volume reduced}$
by an upstream RR BMP	by an upstream RR BMP
Swale slopes less than 2% 1	Swale slopes less than 1% 1
On-line design	Off-line swale cells
No planting	Wetland planting within swale cells
Turf cover in buffer	Trees within swale cells

Wet Swales are generally recommended only for flat coastal plain conditions with a high water table. A linear wetland is always preferred to a wet swale. However, check dams or other design features that lower the effective longitudinal grade of the swale can by applied on steeper sites, to comply with these criteria.



Wet swale

Source: http://www.semcog.org/data/lid.report.cfm?lid=174

Stormwater Functions Summary

Wet swale

Source: http://www.mortonroberts.com/suds.html

Table 11.1. Summary of Stormwater Functions Provided by Wet Swales

Stormwater Function	Level 1 Design	Level 2 Design			
Annual Runoff Volume Reduction (RR)	0%	0%			
Total Phosphorus (TP) EMC Reduction ¹ by BMP Treatment Process	20%	40%			
Total Phosphorus (TP) Mass Load Removal	20%	40%			
Total Nitrogen (TN) EMC Reduction by BMP Treatment Process	25%	35%			
Total Nitrogen (TN) Mass Load Removal	25%	35%			
Channel Protection	Limited – reduced Time of Concentration (TOC); and partial Channel Protection Volume (CPv) can be provided above the Treatment Volume (T _v), within the allowable maximum ponding depth.				
Flood Mitigation	Limited – reduced TOC				

Sources: CWP and CSN (2008), CWP, 2007

Specification No. 12: Filtering Practices

What is it?

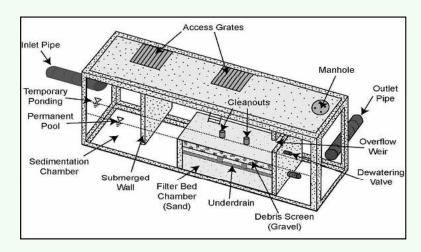
Practices that capture and treat runoff through an engineered storage media. May include:

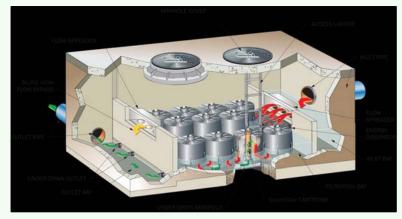
- Non-structural sand filters;
- Surface sand filters;
- Organic media filters;
- Underground sand filters;
- Perimeter sand filters; and
- Proprietary media filters.



Surface sand filter
Source: http://www.cityofsandy.com/index.asp

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Filtering	1	0	30	30	60	60
Practices	2	0	45	45	65	65





Proprietary media filters

Source (top): DCR Stormwater Design Spec No. 11

Source (bottom):

http://www.hiwtc.com/photo/products/11/00/69/6943.jpg

Specification No. 12: Filtering Practices (cont.)

Stormwater Functions Summary

Table 12.1. Summary of Stormwater Functions Provided by Filtering Practices

Stormwater Function	Level 1 Design	Level 2 Design			
Annual Runoff Volume Reduction (RR)	0%	0%			
Total Phosphorus (TP) EMC Reduction ¹ by BMP Treatment Process	60%	65%			
Total Phosphorus (TP) Mass Load Removal	60% 65%				
Total Nitrogen (TN) EMC Reduction by BMP Treatment Process	y 30% 45%				
Total Nitrogen (TN) Mass Load Removal	30% 45%				
Channel Protection	Limited – The Treatment Volume diverted off-line into a storage facility for treatment can be used to calculate a Curve Number (CN) Adjustment.				
Flood Mitigation	None. Most filtering practices are off-line and do not materially change peak discharges.				
¹ Change in the event mean concentration (EMC) through the practice					

Design Criteria

Table 12.2. Filtering Practice Design Guidance

Level 1 Design (RR:0; TP:60; TN:30)	Level 2 Design (RR:0 1; TP:65; TN:45)			
$T_V = [(1.0)(RV)(A)] / 12 - the volume reduced by$	$T_{v} = [(1.25)(Rv)(A)] / 12 - the volume reduced by$			
an upstream BMP	an upstream BMP			
One cell design	Two cell design			
Sand media	Sand media with an organic layer			
Contributing Drainage Area (CDA) contains	CDA is nearly 100% impervious			
pervious area				

¹ May be increased if the 2nd cell is utilized for infiltration in accordance with Stormwater Design Specification No. 8 (Infiltration) or Stormwater Design Specification No. 9 (Bioretention). The Runoff Reduction (RR) credit should be proportional to the fraction of the T_V designed to be infiltrated.



Sand filter below turf Source: http://www.kiama.nsw.gov.au/ environmental-services/water.html

Specification No. 13: Constructed Wetlands

What is it?

Shallow depressions that promote evapotranspiration and microbial activity. May be:

- Constructed wetland basin;
- Multi-cell wetland; and
- Pond/wetland combinations.
- (Extended detention wetlands and pocket wetlands are no longer allowed.)



Constructed wetland typical section and plan views DCR Stormwater Design Spec No. 13





Constructed wetland in Loudoun County Source: Wetland Studies and Solutions, Inc.

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Constructed	1	0 *	25	25	50	50
Wetlands	2	0 *	55	55	75	75

*Note that constructed wetlands do not receive runoff reduction credit, but Level 2 extended detention ponds do! (See slide 70)

Specification No. 13: Constructed Wetlands (cont.)

Design Criteria



Constructed wetland in Fairfax County
Source: Wetland Studies and Solutions, Inc.

Level 1 Design (RR:0; TP:50; TN:25)	Level 2 Design (RR:0; TP:75; TN:55)
$T_{\vee} = [(R_{\vee})(A)] \ / \ 12$ – the volume reduced by an upstream BMP	Tv = $[1.5(R_v)(A)]/12$ – the volume reduced by an upstream BMP
Single cell (with a forebay) ^{1,2}	Multiple cells or a multi-cell pond/wetland combination ^{1,2}
Extended Detention (ED) for T _V (24 hr) ³ or Detention storage (up to 12 inches) above the wetland pool for channel protection (1-year storm event)	No ED. (limited water surface fluctuations allowed during the 1-inch and 1-year storm events – refer to Section 6)
Uniform wetland depth 4	Diverse microtopography with varying depths 2
Mean wetland depth is more than 1 foot	Mean wetland depth is less than 1 foot
The surface area of the wetland is <i>less</i> than 3% of the contributing drainage area (CDA).	The surface area of the wetland is more than 3% of the CDA.
Length/Width ratio OR Flow path = 2:1 or more	Length/Width ratio OR Flow path = 3:1 or more
Length of shortest flow path/overall length = 0.5 or more ³	Length of shortest flow path/overall length = 0.8 or more 4
Emergent wetland design	Mixed wetland design

Stormwater Functions Summary

Table 13.1. Summary of Stormwater Functions Provided by Constructed Wetlands

Stormwater Function	Level 1 Design	Level 2 Design	
Annual Runoff Volume Reduction (RR)	0%	0%	
Total Phosphorus (TP) EMC Reduction ¹ by BMP Treatment Process	50%	75%	
Total Phosphorus (TP) Mass Load Removal	50%	75%	
Total Nitrogen (TN) EMC Reduction by BMP Treatment Process	25%	55%	
Total Nitrogen (TN) Mass Load Removal	25%	55%	
Channel Protection	Yes. Up to 1 foot of detention storage volume can be provided above the normal pool.		
Flood Mitigation	Yes. Flood control storage can be provided above the normal pool.		
Change in event mean concentration (EM	IC) through the practice.		
Sources: CWP and CSN (2008), CWP, 200	7		



Constructed wetland in Fairfax County Source: Wetland Studies and Solutions, Inc.

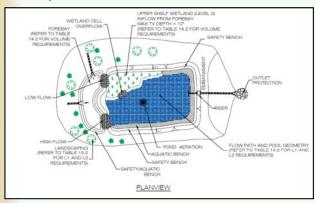
Specification No. 14: Wet Ponds

What is it?

A permanent pool of standing water that promotes settling, biological uptake, and microbial activity. Should be considered only after all other upland runoff reduction options.

May be designed as:

- A single cell;
- Wet extended detention;
- A multi-cell wet pond; or
- A pond/wetland combination.



Wet pond typical plan view DCR Stormwater Design Spec No. 14



Wet pond in Fairfax County Source: Wetland Studies and Solutions, Inc.

Practice	Design Level	Runoff Reduction	TN EMC Removal	TN Mass Load Removal	TP EMC Removal	TP Mass Load Removal
Wet Ponds	1	0	30	30	50	50
vvet Polius	2	0	40	40	75	75

Specification No. 14: Wet Ponds (cont.)



Wet pond in Fairfax County Source: Wetland Studies and Solutions, Inc.

Stormwater Functions Summary

Table 14.1. Summary of Stormwater Functions Provided by Wet Ponds

Stormwater Function	Level 1 Design	Level 2 Design	
Annual Runoff Volume Reduction (RR) 1	0%	0%	
Total Phosphorus (TP) EMC Reduction ² by BMP Treatment Process	50% (45%) ³	75% (65%) ³	
Total Phosphorus (TP) Mass Load Removal	50% (45%) ³	75% (65%) ³	
Total Nitrogen (TN) EMC Reduction ² by BMP Treatment Process	30% (20%) ³	40% (30%) ³	
Total Nitrogen (TN) Mass Load Removal	30% (20%) ³ 40% (30%) ³		
Channel Protection	Yes; detention storage can be provided above the permane pool.		
Flood Mitigation	Yes; flood control storage of permanent pool.	can be provided above	

¹ Runoff Reduction rates for ponds used for year round irrigation can be determined through a water budget computation.

Sources: CWP and CSN (2008), CWP (2007)

Design Criteria

Table 14.2. Level 1 and 2 Wet Pond Design Guidance		
Level 1 Design (RR:0 ¹ ; TP: 50 ⁵ ; TN:30 ⁵)	Level 2 Design (RR:0 ¹ ; TP: 75 ⁵ ; TN:40 ⁵)	
Tv = [(1.0)(Rv)(A)/12] – volume reduced by upstream BMP	Tv = [1.5 (Rv) (A) /12] – volume reduced by upstream BMP	
Single Pond Cell (with forebay)	Wet ED 2 (24 hr) and/or a Multiple Cell Design 3	
Length/Width ratio OR Flow path = 2:1 or more	Length/Width ratio OR Flow path = 3:1 or more	
Length of shortest flow path / overall length ⁴ = 0.5 or more	Length of shortest flow path/overall length ⁴ = 0.8 or more	
Standard aquatic benches	Wetlands more than 10% of pond area	
Turf in pond buffers	Pond landscaping to discourage geese	
No Internal Pond Mechanisms	Aeration (preferably bubblers that extend to or near the bottom or floating islands	

¹ Runoff volume reduction can be computed for wet ponds designed for water reuse and upland irrigation.

Sources: CSN (2009), CWP and CSN (2008), CWP (2007)

² Change in event mean concentration (EMC) through the practice.

³ Note that EMC removal rate is slightly lower in the coastal plain if the wet pond is influenced by groundwater. See Section 6.2 of this design specification and CSN Technical Bulletin No. 2. (2009).

² Extended Detention may be provided to meet a maximum of 50% of the Treatment Volume; Refer to Design Specification 15 for ED design

³ At least three internal cells must be included, including the forebay

⁴ In the case of multiple inflows, the flow path is measured from the dominant inflows (that comprise 80% or more of the total pond inflow)

⁵ Due to groundwater influence, slightly lower TP and TN removal rates in coastal plain (Section 7.2) and CSN Technical Bulletin No. 2. (2009)

Specification No. 15: Extended Detention Ponds

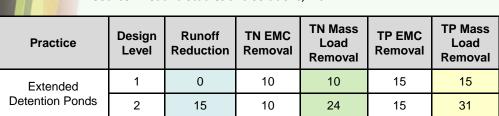
A temporary (12- to 24-hour) pool of standing water that promotes settling after rain events. Should be considered only after all other upland runoff reduction options have been considered.

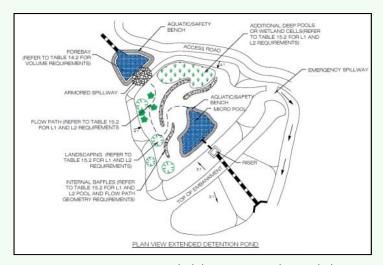
Typical design applications include:

- Micropool extended detention;
- Wet extended detention; or
- Limited extended detention for constructed wetlands.



Extended detention in Fairfax County Source: Wetland Studies and Solutions, Inc.





Extended detention pond typical plan view DCR Stormwater Design Spec No. 15

Specification No. 15: Extended Detention Ponds (cont.)

Stormwater Functions Summary

Table 15.1. Summary of Stormwater Functions Provided by ED Ponds			
Stormwater Function	Level 1 Design	Level 2 Design	
Annual Runoff Volume Reduction (RR)	0%	15%	
Total Phosphorus (TP) EMC	15%	150/	
Reduction by BMP Treatment Process	13%	15%	
Total Phosphorus (TP) Mass Load	15%	31%	
Removal	1070	0170	
Total Nitrogen (TN) EMC Reduction by	10%	10%	
BMP Treatment Process	1070	1070	
Total Nitrogen (TN) Mass Load	10%	24%	
Removal	1.2.0.0		
Channel Protection	Yes; storage volume can be provided to accommodate the		
	full Channel Protection Volume (CP _v)		
Flood Mitigation	Yes; flood control storage can be provided above the		
Flood Mitigation	maximum extended detention volume		

¹ Change in event mean concentration (EMC) through the practice. The actual nutrient mass load removed is the product of the removal rate and the runoff reduction rate (see Table 1 in the *Introduction to the New Virginia Stormwater Design Specifications*).

Sources: CWP and CSN (2008); CWP (2007)

Design Criteria

Table 15.2. Extended Detention (ED) Pond Criteria		
Level 1 Design (RR:0; TP:15; TN:10)	Level 2 Design (RR:15; TP:15; TN:10)	
$T_v = [(1.0) (Rv) (A)] / 12 - the volume reduced by an upstream BMP$	$T_V = [(1.25) (R_V) (A)] / 12$ – the volume reduced by an upstream BMP	
A minumum of 15% of the $T_{\rm V}$ in the permanent pool (forebay, micropool)	A minumum of 40% of T _V in the permanent pool (forebay, micropool, or deep pool, or wetlands)	
Length/Width ratio OR flow path = 2:1 or more	Length/Width ratio OR flow path = 3:1 or more	
Length of the shortest flow path / overall length = 0.4 or more	Length of the shortest flow path / overall length = 0.7 or more	
Average T _v ED time = 24 hours or less	Average T _v ED time = 36 hours	
Vertical T _v ED fluctuation exceeds 4 feet	Maximum vertical T _v ED limit of 4 feet	
Turf cover on floor	Trees and wetlands in the planting plan	
Forebay and micropool	Incudes additional cells or features (deep pools, wetlands, etc.) Refer to Section 5	
CDA is less than 10 acres	CDA is greater than 10 acres	



Extended detention in Fairfax County Source: Wetland Studies and Solutions, Inc.



Virginia Runoff Reduction Method (VRRM)

Background:

Created by the Center for Watershed Protection and the Chesapeake Stormwater Network with funding from the National Fish and Wildlife Foundation and the Virginia DCR.

Spreadsheets and documentation available at: http://www.dcr.virginia.gov/lr2f.shtml (Most recent revision: March 28, 2011)

4VAC50-60-65.A: "Compliance with the water quality design criteria set out in subdivisions 1 and 2 of 4VAC50-60-63 shall be determined by utilizing the Virginia Runoff Reduction Method or another equivalent methodology that is approved by the board."

What does VRRM do?

- VRRM calculates runoff volume and TP load based on land cover and soils;
- User inputs BMP types and coverage;
- VRRM calculates the runoff volume reduction and TP load reduction from BMP coverage; and
- VRRM calculates the adjusted curve numbers for BMP sizing; however, it does not perform the 1-year storm sizing calculations.



Virginia Runoff Reduction Method (VRRM)

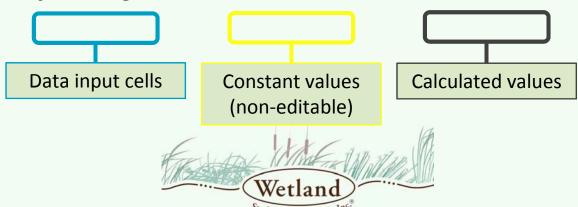
Process Steps:

- Enter project and land cover information. ("Site Data" tab)
- Apply BMPs to the site and review phosphorus load reductions.
 Continue to add additional BMPs until phosphorus load reduction requirements are met.

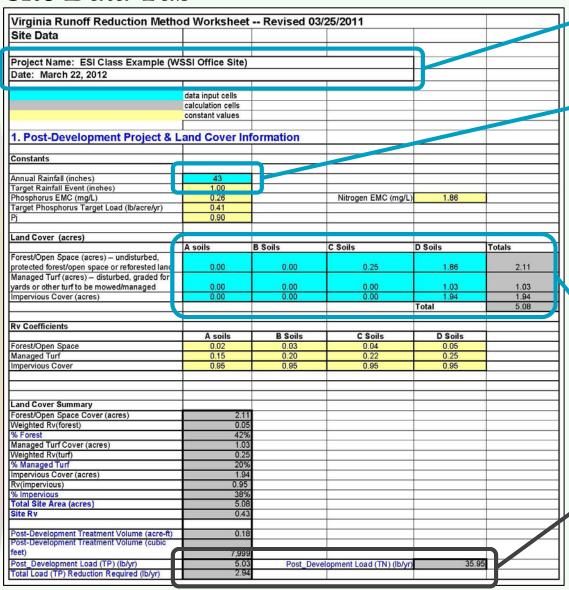
("D.A." and "Water Quality Compliance" tabs)

3. Determine allowable peak flow using adjusted curve numbers. ("Channel and Flood Protection" tab)

Legend for the following VRRM slides:



Site Data Tab



Data Input:

Enter project name/date

Data Input:

Enter annual rainfall

Data Input:

Enter post-development, pre-BMP land cover data. Note that:

- "Forest/Open Space" includes planted meadow which will not be mowed or maintained;
- "Managed Turf" includes areas to be mowed; and
- "Impervious cover" includes BMPs on surfaces that would otherwise be impervious (e.g., green roof, pervious parking.)

See VRRM documentation, Table 1.

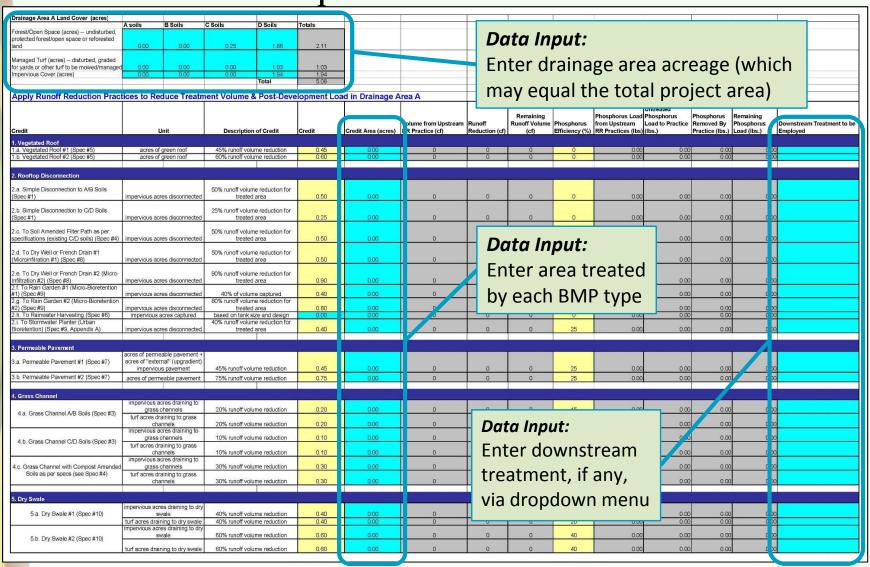
Calculated:

Post-development loads and required reduction

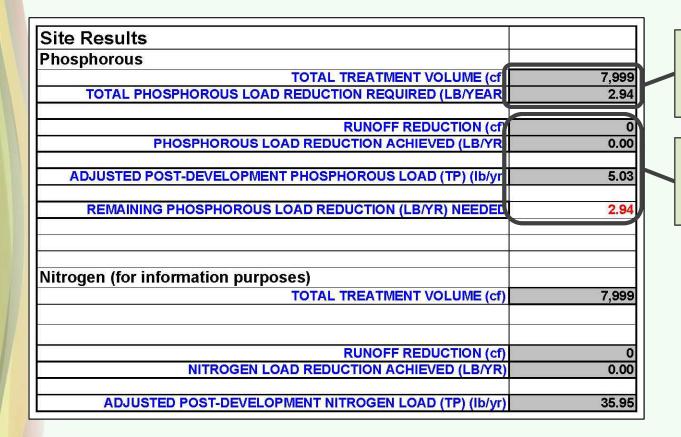
D.A. Tabs-Constant Values

rainage Area A Land Cover (acres)	A soils	B Soils	C Soils	D Soils	Totals										
rest/Open Space (acres) undisturbed,	A SOIIS	B Soils	C Soils	D Solis	iotais										
otected forest/open space or reforested	0.00	0.00	0.25	1.86	2.11										
	0.00	0,00	0,20	1.00	2.11					1					
anaged Turf (acres) disturbed, graded yards or other turf to be mowed/managed	0.00	0.00	0.00	1.03	1.03										
pervious Cover (acres)	0.00	0.00	0.00	1.94	1.94										
* * * * * * * * * * * * * * * * * * * *				Total	5.08										
pply Runoff Reduction Pract	ices to Re	duce Treatr	ment Volume &	Post-Deve	elopment Loa	ad in Drainac	e Area A								
												Untreated	-		
									Remaining		Phosphorus Load	Phosphorus		emaining	
redit	L	Init	Description	of Credit	Credit	C edit Area (acr	Volume from Upstream res) RR Practice (cf)	Runoff Reduction (cf)			t om Upstream F t Practices (Ibs)	Load to Practice (lbs.)	Practice (lbs.) L		Downstream Treatment to I Employed
Vegetated Roof							(-)	(\	(10)					
a. Vegetated Roof #1 (Spec #5)	acres of	green roof	45% runoff volum		0.45	0.00	0	0	0	0	0.00	0.00		0.00	
Vegetated Roof #2 (Spec #5)	acres of	green roof	60% runoff volur	ne reduction	0.60	0.00	0	0	0	0	0.00	0.00	0.00	0.00	
Pooffon Disconnection		h			4			"	dat.	- N			16		
Rooftop Disconnection			<u> </u>			T									
a. Simple Disconnection to A/B Soils pec #1)	in projecte con	es disconnected	50% runoff volume treated:		0.50	0.00	n	0	0	0	0.00	0.00	0.00	0.00	
	m lei vious aci	es disconnected			0,30	0.00	U			0	0.00	0.00	0.00	0.00	
b. Simple Disconnection to C/D Soils pec #1)	in envious acr	es disconnected	25% runoff volume treated		0.25	0.00	n	0	0	0	0.00	0.00	0.00	0.00	
	in ervious acr	es disconnected	Ireated:	ilea	0.25	0.00	U	- 0	-	0	0.00	0.00	0.00	0.00	
c. To Soil Amended Filter Path as per ecifications (existing C/D soils) (Spec #4)	in on doug oor	es disconnected	50% runoff volume treated		0.50	0.00	· <u>~</u> ·		L0	0	0.00	0.00	0.00	0.00	
	III ervious aci	es disconnected			0.50	0.00	_		0	0	0.00	0.00	0.00	0.00	
d. To Dry Well or French Drain #1 licroinfilration #1) (Spec #8)	in on dour nor	es disconnected	50% runoff volume treated:		0.50	0.00	Constan)†·	o	25	0.00	0.00	0.00	0.00	
	III el vious au	es disconnected			0.30	0.00	Constan		-	25	0.00	0.00	0.001	0.00	
e. To Dry Well or French Drain #2 (Micro- filtration #2) (Spec #8)	in ondoue cor	es disconnected	90% runoff volume treated		0.90	0.00	TD Dadu	ction		25	0.00	Con	stant:		
f. To Rain Garden #1 (Micro-Bioretention		es disconnected	il eateu.				TP Redu	CUOI) <mark></mark> -			_ COII	stuiit.		_
1) (Spec #9) g. To Rain Garden #2 (Micro-Bioretention	in ervious ac		_	ed on fo	0.40	0.00			0	25	0.00		C D ~ 4		
2) (Spec #9)	in ervious ac	Con	stant:		0.80	or/	via volu	me	0	50	0.00		C Red	luctio	n via
h. To Rainwater Harvesting (Spec #6) i. To Stormwater Planter (Urban	npervious			esign on fo	0.00	.00			0	0	0.00	<u> </u>			_
oretention) (Spec #9, Appendix A)	in ervirus ac	RI//I	P Type	onito	0.40	0.00	reduction	n	o	25	0.00	che	mical	proc	esses
har and a		וועוט	riype				reduction	/11						•	_
Permeable Pavement	ac as of perme	able navement +			7			1		_		- (red	ductio	n tak	en on
a. Permeable Pavement #1 (Spec #7)	ac es of "exter	nal" (upgradient)			200,000					100		(100	auctio	iii tan	CII OII
b. Permeable Pavement #2 (Spec #7)		s pavement	45% runoff volum		0.45	0.00	0	0	0	25	0.00	- KO 10	alaia	باميرم	
b. Permeable Pavement #2 (Spec #1)	a es of perm	eable pavement	75% runoff volum	ne reduction	0.75	0.00	0	0	0	25	0.00	– ren	nainin	g voi	ume) <mark>-</mark>
Grass Channel		*	A		A)			**	*//						
		cres draining to	20% runoff volui	no rodustice	0.20	0.00	0	0	0	15	0,00	0.00	0.00	0.00	
4.a. Grass Channel A/B Soils (Spec #3)		channels aining to grass											*		
	cha	nnels cres draining to	20% runoff volui	ne reduction	0.20	0.00	0	0	0	15	0.00	0.00	0.00	0.00	
4 h Come Channel C/D Calls (Come #2)		channels	10% runoff volui	ne reduction	0.10	0.00	0	0	0	15	0.00	0.00	0.00	0.00	
4.b. Grass Channel C/D Soils (Spec #3)	urf acres dri	aining to grass				2.00			_		0.44	0.00			
		nnels cres draining to	10% runoff volui	ne reduction	0.10	0.00	0	0	0	15	0.00	0.00		0.00	
c. Grass Channel with Compost Amended	grass o	channels	30% runoff volu	ne reduction	0.30	0.00	0	0	0	15	0.00	0.00	0.00	0.00	
Soils as per specs (see Spec #4)		aining to grass nnels	30% runoff volui	ne reduction	0.30	0.00	0	0	0	15	0.00	0.00	0.00	0.00	
	One		Service Fold		3.00		-				0.00	0.00	0,00	0,00	
Dry Swale															
5.a. Dry Swale #1 (Spec #10)		es draining to dry vale	40% runoff volui	no reduction	0.40	0.00	n	0	0	20	0.00	0.00	0.00	0.00	
		vale ning to dry swale			0.40	0.00	0	0	0	20	0.00	0.00		0.00	
LONG THE	im ervious acn	es draining to dry	/			0.00	0	0	0	40	0.00	0.00		0.00	
5.b. Dry Swale #2 (Spec #10)	SV	vale	60% runoff volu		0.60			0			20.000				
		ning to dry swale	60% runoff volui		0.60	0.00	0	0	0	40	0.00	0.00	0.00	0.00	

D.A. Tabs - User Input



Water Quality Compliance Tab

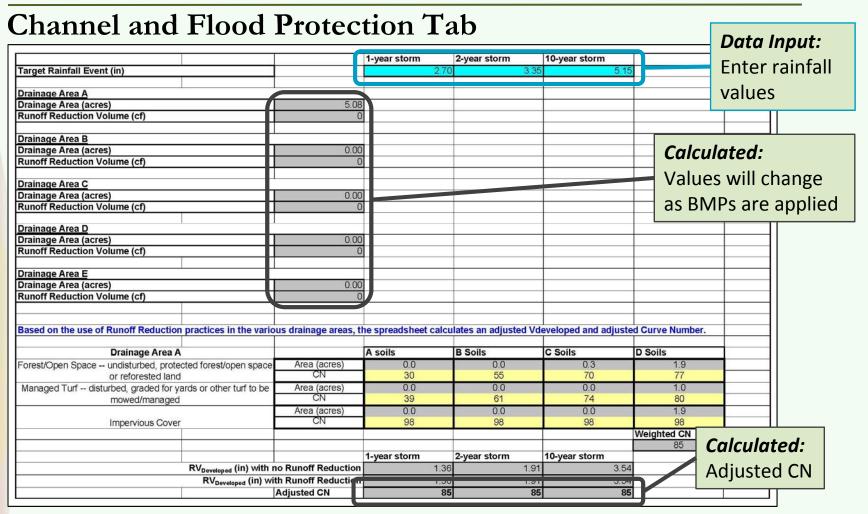


Calculated:

Static values based on Land Cover tab

Calculated:

Values will change as BMPs are applied



Using the adjusted curve number (CN) for each drainage area, calculate the peak discharge for the 1-, 2-, and 10-year storms. Compare the peak discharge to the allowable rates described in the Virginia Stormwater Management Program permit regulations (4VAC 50-60-66(b) 4VAC 50-60-66(c)).

Channel Protection using TR-55 and Energy Balance

To meet the requirements of 4VAC50-60-66.B (Channel Protection), use the adjusted curve numbers from the VRRM to determine the pre- and post-development runoff volume and the pre-development runoff rate.

```
RV_{pre/post-developed} = Q \times A / 12
```

Where:

RV = Runoff volume (cf)

A = Drainage area (sf)

 Q_{depth} = Runoff (in) = $(P-1)^2$

$$= \frac{(P-I_a)^2}{(P-I_a) + S}$$

Where:

P = Precipitation (in)

I_a = Initial abstraction

= 0.2S

= (1000 / CN) - 10

 $Q_{\text{pre-developed}} = q_{\text{u}} \times A_{\text{m}} \times Q_{\text{depth}} \times F_{\text{p}}$

Where:

Q_{pre-developed} = Peak discharge (cfs)

q_u = Unit peak discharge (csm/in)

(Determined using the graphical peak discharge method or tabular hydrograph method. See TR-55.)

 $A_m = Drainage area (mi²)$

 Q_{denth} = Runoff (in)

F_n = Pond and swamp adjustment factor

Channel Protection using TR-55 and Energy Balance

Solve for the allowable $Q_{developed}$ using the Energy Balance method (4VAC50-60-66.B) and the values calculated on the previous slide.

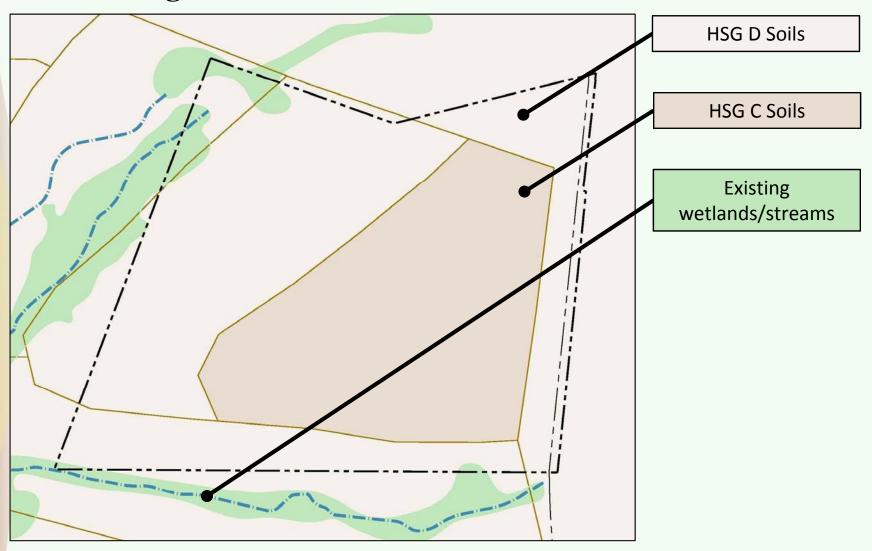
Allowable 1-yr, 24-hr peak flow rate per 4VAC50-60-66.B: $Q_{developed} \leq 0.8 \times Q_{pre-developed} \times RV_{pre-developed} / RV_{developed}$ $Q_{developed} \text{ shall not be required to be less than } [Q_{forested} \times RV_{forested}] / RV_{developed}$ $Q_{developed} \text{ must be } \leq Q_{pre-developed}$

Introduction

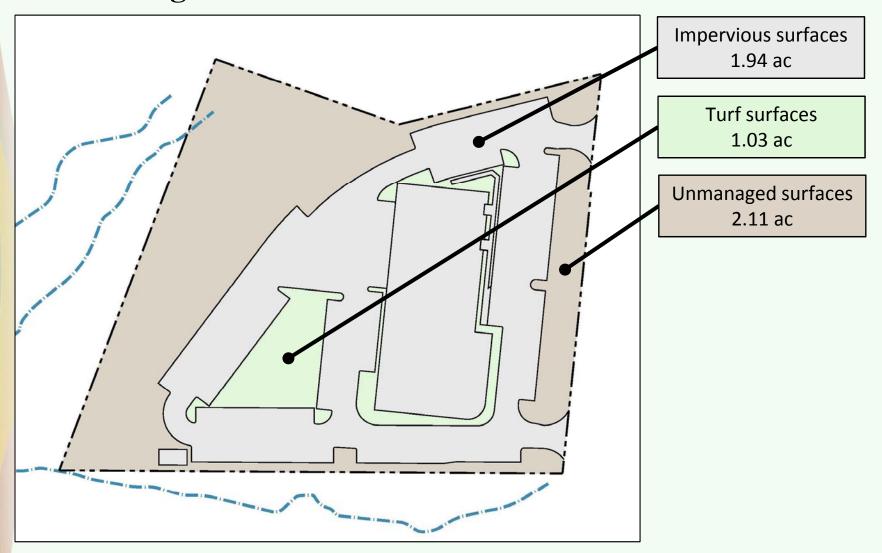
This example is based on WSSI's office site. However, this is a simplified analysis for VRRM process illustration purposes only.

Note that the site's drainage areas have been changed, and not all practices currently on the ground at WSSI are represented herein.

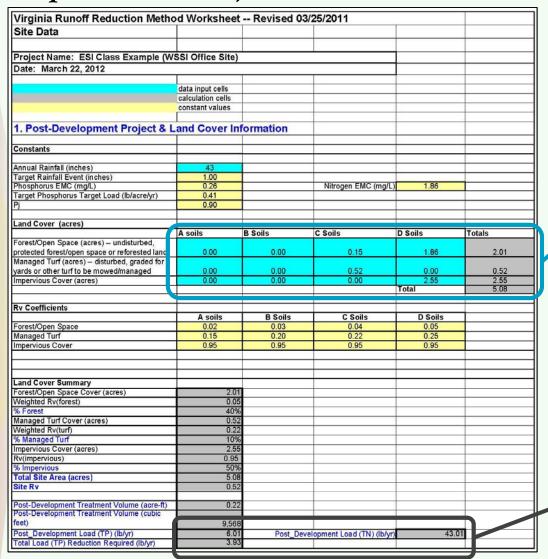
Initial Design Information: Base Land Cover



Initial Design Information: Pre-BMP Plan



Step 1: Enter Project and Land Cover Information



Enter land cover data

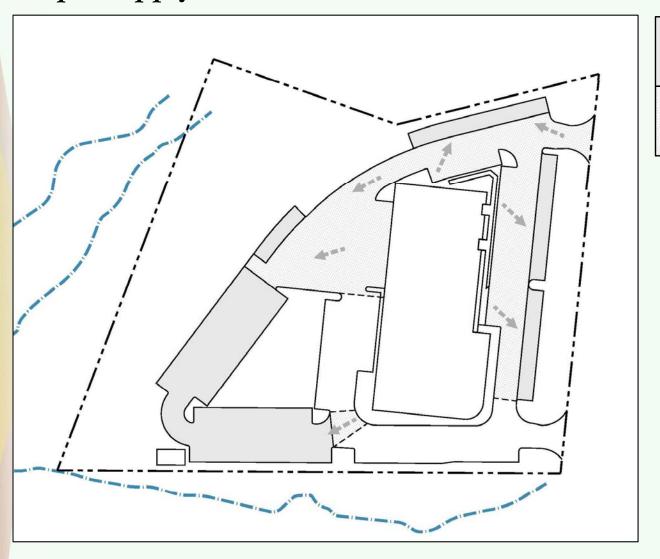
Post-development TP load:

6.01 lb/yr

Required TP reduction:

3.93 lb/yr

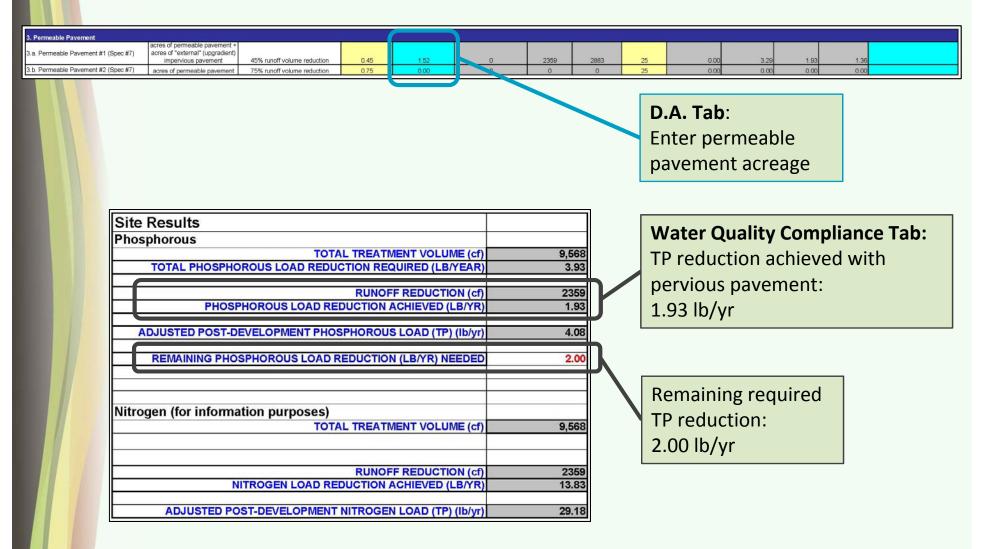
Step 2: Apply BMPs- Level 1 Pervious Pavement



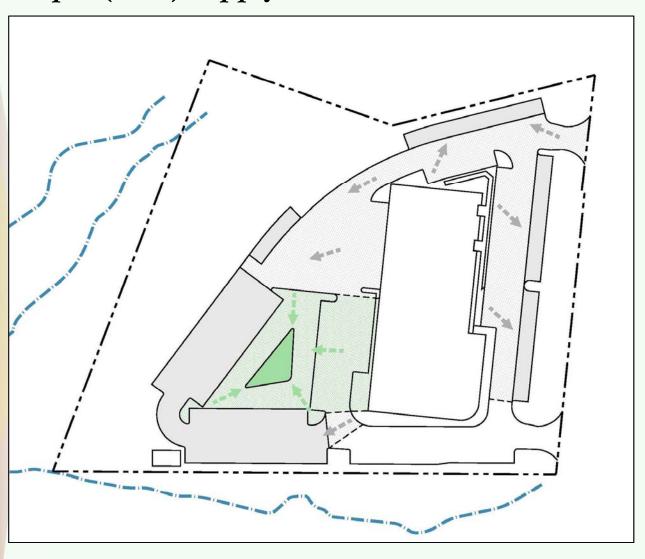
L1 Pervious pavement 0.67 ac

0.85 "up-gradient" impervious acres

Step 2 (cont): Apply BMPs; Review Phosphorus Reduction



Step 2 (cont): Apply BMPs- Level 1 Bioretention



L1 Pervious pavement 0.67 ac

0.85 "up-gradient" impervious acres

L1 Bioretention

0.17 "up-gradient" impervious acres

0.25 "up-gradient" turf/impervious acres

Step 2 (cont): Apply BMPs; Review Phosphorus Reduction

6. Bioretention													
6.a Bioretention #1 or Urban Bioretention (Spec #9)	impervious acres draining to bioretention 40% runoff volume reduction turf acres draining to bioretention 40% runoff volume reduction		0.40	0.17	0	234	352	25	0.00	0.37	0.20	0.17	
			0.40	0.29	0	93	139	25	0.00	0.15	0.08	0.07	
6 b. Bioretention #2 (Spec #9)	impervious acres draining to bioretention	80% runoff volume reduction	0.80	0.00	0	0	0	50	0.00	0.00	0.00	0.00	
	turf acres draining to bioretention	80% runoff volume reduction	0.80	0.00	0	0	0	50	0.00	0.00	0.00	0.00	

D.A. Tab:

Enter bioretention watershed acreage

Site Results Phosphorous **TOTAL TREATMENT VOLUME (cf)** 9,568 TOTAL PHOSPHOROUS LOAD REDUCTION REQUIRED (LB/YEAR) 3.93 2686 RUNOFF REDUCTION (cf) PHOSPHOROUS LOAD REDUCTION ACHIEVED (LB/YR) 2.21 ADJUSTED POST-DEVELOPMENT PHOSPHOROUS LOAD (TP) (lb/yr) 3.80 REMAINING PHOSPHOROUS LOAD REDUCTION (LB/YR) NEEDED 1.71 Nitrogen (for information purposes) TOTAL TREATMENT VOLUME (cf) 9,568 RUNOFF REDUCTION (cf) 2686

NITROGEN LOAD REDUCTION ACHIEVED (LB/YR)

ADJUSTED POST-DEVELOPMENT NITROGEN LOAD (TP) (lb/yr)

Water Quality Compliance Tab:

TP reduction achieved with pervious pavement and bioretention:

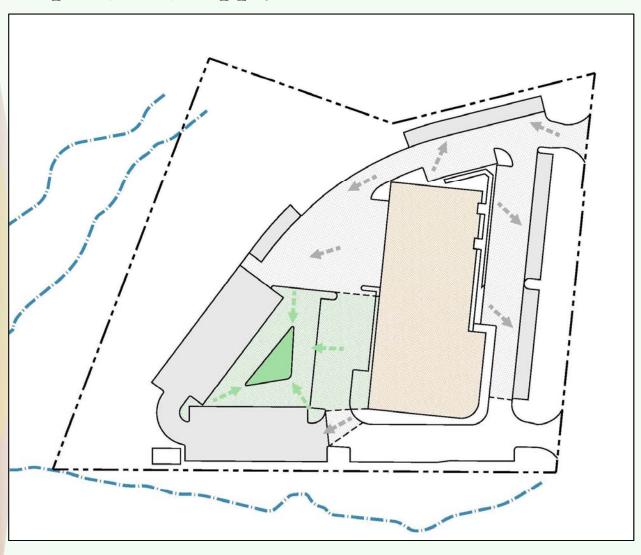
2.21 lb/yr

16.18

26.83

Remaining required TP reduction: 1.71 lb/yr

Step 2 (cont): Apply BMPs- Rainwater Harvesting



L1 Pervious pavement 0.67 ac

0.85 "up-gradient" impervious acres

L1 Bioretention

0.17 "up-gradient" impervious acres

0.25 "up-gradient" turf/impervious acres

Harvesting 0.59 roof acres

Apply BMPs- Rainwater Harvesting Spreadsheet

-PP-J	
Input	
REGIONAL LOCATION	
What region will the rainwater harvesting system be located closest to?	2
click drop down menu in green on the right for directions to appear)	
ROOF AREA	
How big is the roof footprint (in sf)?	25,700
IRRIGATION	
What is the daily demand for irrigation in gallons? (if you do not know the daily	
demand, use the next two questions to generate an estimated demand)	0
How big is the area to irrigate?	30,500
How many inches per week of irrigation are needed?	1.00
What day of the year does irrigation start?	120
What day of the year does irrigation end?	270
Total daily irrigation demand (gallons)	2,701
INDOOR DEMAND - FLUSING TOILETS/URINALS	
Water closet and urinal use (if only toilets are used, set urinals = 0)	0.1920
How many people will use the building?	120
How much water does each urinal use? (set to 0, if no urinal)	0.00
How much water does each toilet use?	1.10
Calculated daily water closet and urinal demand in gallons (if this has already been	8
calculated, use this instead of the rows above)	0
Start day of the week (Monday=1, etc)	1
End day of the week (Monday=1, etc)	5
Hours per day the building is used (i.e. 8 for a 9-5 office building; 24 for a shift-	0
work factory)	9
Total daily water closet and urinal demand (gallons)	297
INDOOR DEMAND - LAUNDRY	
Laundry use (use either loads per day, pounds per day or calculated demand)	
How many loads of laundry are done each day?	0
How much water does each load of laundry use in gallons?	42
How many pounds of laundry are done per day?	0
Calculated daily laundry demand	
Start day of the week (Monday=1, etc)	1 5
End day of the week (Monday=1, etc)	0
Total daily laundry demand (gallons)	Ü
ADDITIONAL DAILY USE	
Additional daily use (bus wash, street sweepers, etc) in gallons	
Daily use in gallons	0
Start day of the week (Monday=1, etc)	1
End day of the week (Monday=1, etc)	7
Total daily additional demand (gallons)	0
CHILLED WATER COOLING TOWERS	
If water is to be used for cooling towers (for large scale projects)	
Start day of the week (Monday=1, etc)	1
End day of the week (Monday=1, etc)	7
Total daily water cooling tower demand (gallons)	0
SECONDARY RUNOFF REDUCTION DRAWDOWN	
How many gallons per day are directed to the secondary practice?	0
What day of the year does secondary practice start?	1
What day of the year does secondary practice end?	366
Total daily additional demand (gallons)	0
FIRST FLUSH FILTER DIVERSION AND EFFICIENCY	
Filter Efficiency must be MIN 95% of 1" storm for Treatment Volume Credit	
and MIN 95% of 2 year storm for Channel Protection Credit. This value may	
be modified if higher efficiencies are realized	
Filter Efficiency Associated with the 1" storm	0.05
This spreadsheet was prepared for use by the Department of Conservation and Recreation. All rights are re-	served by the Author
of the spreadsheet. It may not be modified or used beyond DCR's intended use without prior written consent	of the Authors.

Enter water usage information

Determine runoff reduction credit based on cistern size

Cistern Storage Associated with Treatment Volume Credit (gallons)	Overflow frequency for storms of 1" or less (per year)	Dry Frequency	Mean Overflow of 1" storm volume per year (thousands of gallons)	Runoff Reductio Volume Credit		
10,000	47%	28%	165	40%		
20,000	43%	25%	153	43%		
20,000	410/	220/	147	150/		
40,000	40%	21%	142	46%		
50,000	38%	20%	136	48%		
60,000	37%	19%	130	49%		
70,000	36%	18%	125	51%		
80,000	34%	17%	119	52%		
90,000	33%	16%	114	53%		
100,000	31%	15%	109	55%		
110,000	30%	14%	104	56%		
120,000	29%	13%	98	58%		
130,000	27%	12%	92	59%		
140,000	25%	11%	86	61%		
150,000	23%	10%	82	62%		
160,000	22%	10%	78	63%		
170,000	20%	9%	73	64%		
180,000	19%	8%	69	65%		

(Spreadsheet available at

http://vwrrc.vt.edu/swc/NonProprietaryBMPs.html).

Step 2 (cont): Apply BMPs; Review Phosphorus Reduction

2.a. Simple Disconnection to A/B Soils Spec #1)	impervious acres disconnected	50% runoff volume reduction for treated area	0.50	0.00	0	0	0	0 0.00 0.00 0.00	0.00
2.b. Simple Disconnection to C/D Soils (Spec #1)	impervious acres disconnected	25% runoff volume reduction for treated area	0.25	0.00	0	0	0	000 000	0.00
e.c. To Soil Amended Filter Path as per specifications (existing C/D soils) (Spec #4)	impervious acres disconnected	50% runoff volume reduction for treated area	0.50	0.00	0	0	0	D.A. Tab:	0.00
d. To Dry Well or French Drain #1 Microinfilration #1) (Spec #8)	impervious acres disconnected	50% runoff volume reduction for treated area	0.50	0.00	0	0	0	Enter roof acreage and	0.00
2.e. To Dry Well or French Drain #2 (Micro- nfiltration #2) (Spec #8)	impervious acres disconnected	90% runoff volume reduction for treated area	0.90	0.00	0	0	0	harvesting credit from	0.00
	impervious acres disconnected	40% of volume captured	0.40	0.00	0	0	0	_	0.00
.g. To Rain Garden #2 (Micro-Bioretention 2) (Spec #9)	impervious acres disconnected	80% runoff volume reduction for treated area	0.80	0.00	U	0	0	harvesting spreadsheet	
	impervious acres captured		0.41	0.59	0	834	1200	_ · · · · · · · · · · · · · · · · · · ·	0.75
2.f. To Rain Garden #1 (Micro-Bioretention #1) (Spec #9) 2.g. To Rain Garden #2 (Micro-Bioretention #2) (Spec #9) 2.h. To Rainwater Harvesting (Spec #6) 2.t. To Stormwater Planter (Urban	impervious acres disconnected	40% of volume captured 80% runoff volume reduction for	0.40	0.00	0	0 0 834	0 0 1200	harvesting spreadsheet	0.00 0.00 0.75

Site Results	
Phosphorous	
TOTAL TREATMENT VOLUME (cf)	9,568
TOTAL PHOSPHOROUS LOAD REDUCTION REQUIRED (LB/YEAR)	3.93
RUNOFF REDUCTION (cf)	3520
PHOSPHOROUS LOAD REDUCTION ACHIEVED (LB/YR)	2.74
ADJUSTED POST-DEVELOPMENT PHOSPHOROUS LOAD (TP) (lb/yr)	3.27
REMAINING PHOSPHOROUS LOAD REDUCTION (LB/YR) NEEDED	1.19
REMAINING PHOSPHOROUS LOAD REDUCTION (LB/YR) NEEDED	1.19
REMAINING PHOSPHOROUS LOAD REDUCTION (LB/YR) NEEDED Nitrogen (for information purposes)	1.19
	9,568
Nitrogen (for information purposes)	
Nitrogen (for information purposes) TOTAL TREATMENT VOLUME (cf)	9,568
Nitrogen (for information purposes) TOTAL TREATMENT VOLUME (cf) RUNOFF REDUCTION (cf)	9,568
Nitrogen (for information purposes) TOTAL TREATMENT VOLUME (cf)	9,568

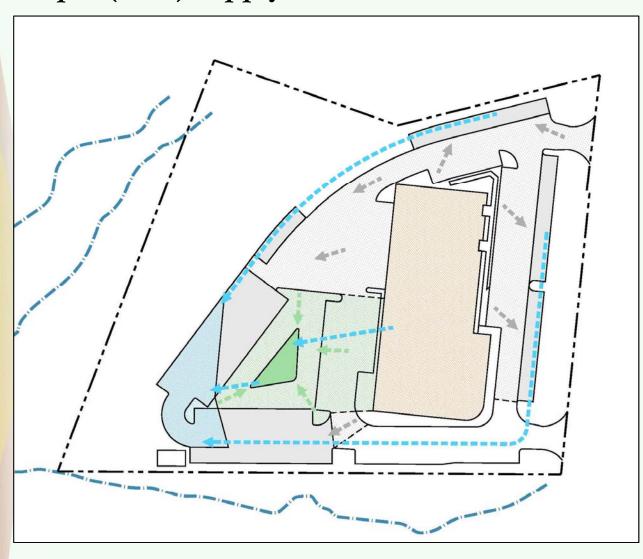
Water Quality Compliance Tab:

TP reduction achieved with pervious pavement, bioretention, and harvesting:

2.74 lb/yr

Remaining required TP reduction: 1.19 lb/yr

Step 2 (cont): Apply BMPs- Downstream Treatment



L1 Pervious pavement 0.67 ac

0.85 "up-gradient" impervious acres

L1 Bioretention

0.17 "up-gradient" impervious acres

0.25 "up-gradient" turf/impervious acres

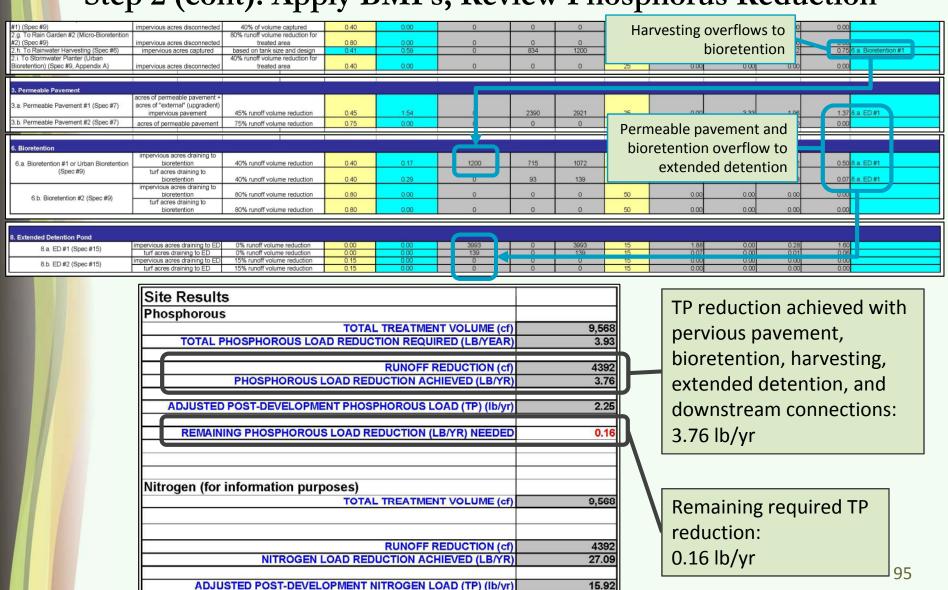
Harvesting

0.59 roof acres

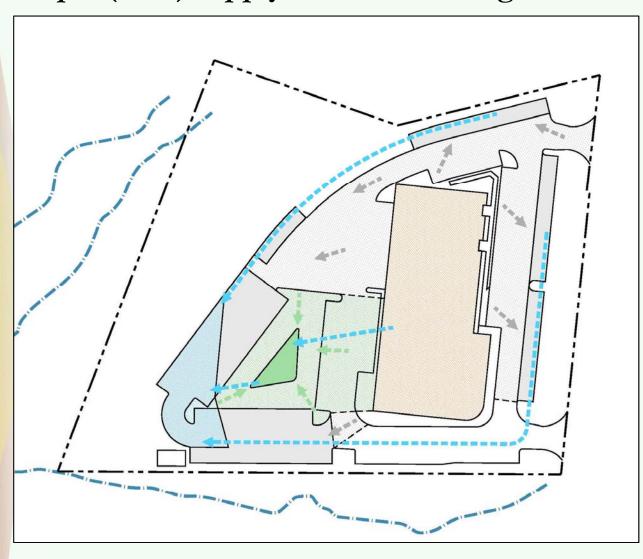
L1 Extended Detention

Accepts overflow from upstream practices via underdrains

Step 2 (cont): Apply BMPs; Review Phosphorus Reduction



Step 2 (cont): Apply BMPs- Re-design Pavement to Level 2



L2 Pervious pavement 0.67 ac

0.85 "up-gradient" impervious acres

L1 Bioretention

0.17 "up-gradient" impervious acres

0.25 "up-gradient" turf/impervious acres

Harvesting

0.59 roof acres

L1 Extended Detention

Accepts overflow from upstream practices via underdrains

Step 2 (cont): Apply BMPs; Review Phosphorus Reduction

3. Permeable Pavement													
3.a. Permeable Pavement #1 (Spec #7)	acres of permeable pavement + acres of "external" (upgradient) impervious pavement		0.45	0.67	0	1040	1271	25	0.00	1.45	0.85	0.60	8.a. ED#1
3.b. Permeable Pavement #2 (Spec #7)	acres of permeable pavement	75% runoff volume reduction	0.75	0.85	9	2198	733	25	0.00	1.84	1.49	0.34	8.a. ED #1
							_						

D.A. Tab:

Design permeable pavement to Level 2 specifications

Site Results		
Phosphorous	0.500	ı
TOTAL TREATMENT VOLUME (cf) TOTAL PHOSPHOROUS LOAD REDUCTION REQUIRED (LB/YEAR)		41
RUNOFF REDUCTION (cf) PHOSPHOROUS LOAD REDUCTION ACHIEVED (LB/YR)		
ADJUSTED POST-DEVELOPMENT PHOSPHOROUS LOAD (TP) (lb/yr)	1.92	Γ
REMAINING PHOSPHOROUS LOAD REDUCTION (LB/YR) NEEDED	CONGRATULATIONS!! YOU EXCEEDED THE TARGET REDUCTION BY 0.2 LB/YEAR!!	
Nitrogen (for information purposes) TOTAL TREATMENT VOLUME (cf)	9,568	
RUNOFF REDUCTION (cf)		
NITROGEN LOAD REDUCTION ACHIEVED (LB/YR) ADJUSTED POST-DEVELOPMENT NITROGEN LOAD (TP) (Ib/yr)		
ADJUSTED POST-DEVELOPMENT NITROGEN LOAD (TP) (lb/yr)	13.45	

Water Quality Compliance Tab:

TP reduction achieved with Level 2 pervious pavement, bioretention, harvesting, extended detention, and downstream connections:
4.09 lb/yr

TP Reduction requirement met via:

Level 2 pervious pavement;

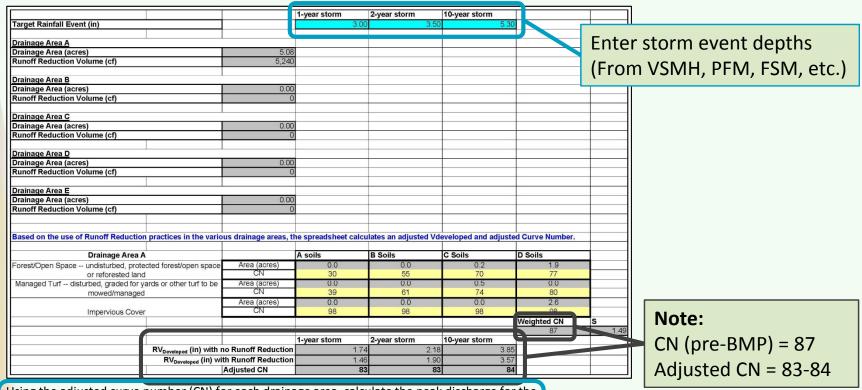
Level 1 bioretention;

Harvesting (for irrigation and toilets);

Extended detention; and

Downstream connections.

Step 3: Determine Allowable Peak Flow



Using the adjusted curve number (CN) for each drainage area, calculate the peak discharge for the 1-, 2-, and 10-year storms. Compare the peak discharge to the allowable rates described in the Virginia Stormwater Management Program permit regulations (4VAC 50-60-66(b) and (c)).

Use adjusted CNs to determine the site's runoff volume and peak discharge. Compare to the requirements of 4VAC50-60-66.B.

Runoff Volume Estimation Using TR-55

Step 1. Solve for RV_{pre-development} and RV_{post-development} for use in the Energy Balance method (4VAC50-60-66.B).

Pre-development Runoff Volume Calculations:

$$Q_{depth} = [(P - 0.2S)^2] / [(P + 0.8S)]$$

$$= [(3.0 - (0.2 \times 3.16))^2] / [(3.0 + (0.8 \times 3.16))]$$

$$= 1.0 \text{ in}$$

$$RV_{pre-development} = Q \times A / 12$$

= 1.0" x 221,284 sf / 12"

$$RV_{pre-development}$$
 = 18,440 cf

Pre-development condition assumptions for this example:

- Land cover is forest in good condition
- Weighted CN = 76
- 1-year rainfall event = 3.0" (per VSMH Table 4B)

Post-development Runoff Volume Calculations:

$$Q_{depth} = [(P - 0.2S)^2] / [(P + 0.8S)]$$

= $[(3.0 - (0.2 \times 2.05))^2] / [(3.0 + (0.8 \times 2.05))]$
= 1.5 in (Note that this is also given in the VRRM spreadsheet)

$$RV_{post-development} = Q \times A / 12$$

$$RV_{post-development} = 27,660 \text{ cf}$$

Post-development conditions for this example:

- See Slide 97 for adjusted post-development CN
- Adjusted CN = 83 (1-yr storm)
- 1-year storm= 3.0" (per VSMH Table 4B)

Note that Rv_{post-development pre-BMP} = 32,115 cf Post-development, Pre-BMP CN = 87

Pre-Development Peak Flow Estimation Using TR-55

Step 2. Solve for Q_{pre-developed} for use in the Energy Balance method (4VAC50-60-66.B).

$$Q_{pre-developed} = q_u \times A_m \times Q_{depth} \times F_p$$

$$q_{ij} = 520 \text{ csm/in}$$

For graphical peak discharge method:

$$I_a = 0.2 \times ((1000/83) - 10) = 0.41$$

$$I_a / P = 0.41 / 3.0 = 0.14$$

$$A_{\rm m}$$
 = 221,284 sf = 0.008 mi²

$$F_{\rm p} = 1.0$$

$$Q_{pre-developed} = 520 \times 0.008 \times 1.0 \times 1.0$$

$$Q_{pre-developed} = 4.2 cfs$$

Assumptions for this example:

- $T_c = 0.5 \text{ hr}$
- Rainfall distribution = SCS Type II
- 1-year rainfall event = 3.0" (per VSMH Table 4B)
- q₁₁ determined from graphical peak discharge method
- $F_p = 1.0$

Channel and Flood Protection – Allowable Peak Flow

Step 3. Solve for the allowable Q_{developed} using the Energy Balance method (4VAC50-60-66.B).

```
Allowable 1-yr, 24-hr peak flow rate per 4VAC50-60-66.B: Q_{developed} \leq 0.8 \times Q_{pre-developed} \times RV_{pre-developed} / RV_{developed} Q_{developed} \text{ shall not be required to be less than } [Q_{forested} \times RV_{forested}] / RV_{developed} Q_{developed} \text{ must be } \leq Q_{pre-developed}
```

```
Q_{pre-developed} = 4.2 cfs (See slide 99. Also equals Q_{forested} in this example.) RV_{pre-developed} = 18,440 cf (See slide 98. Also equals RV_{forested} in this example) RV_{developed} = 27,660 cf (See slide 98.)
```

Applying the Energy Balance Method conditions above:

References

Stormwater Regulations

- http://www.dcr.virginia.gov/documents/swmfinregspublishedvareg.pdf
- (Additional information: http://www.dcr.virginia.gov/lr2d.shtml)

Virginia Runoff Reduction Method

http://www.dcr.virginia.gov/lr2f.shtml

Virginia Stormwater BMP Clearinghouse

http://vwrrc.vt.edu/swc/

